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ANALYSIS OF SHOCKS BY NUMERICAL SOLUTION
OF DUHAMEL'S INTEGRAL

CALEDONIA L. HENRY

DECEMBER 1988

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U.S. ARMY LABORATORY COMMAND

BALLISTIC RESEARCH LABORATORY
ABERDEEN PROVING GROUND, MARYLAND

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I. INTRODUCTION

Some of the ongoing concerns of the Weapon Dynamics and Accuracy Branch (WDAB) of the Interior Ballistics Division (IBD) of the Ballistic Research Laboratory (BRL) are

- (1) To realistically test instrumentation and structures for survivability and reliability in gun launch environments,
- (2) To assess the damage to the human ear due to nonclassical pressure pulses such as those generated by multiple sources in confined volumes,
- (3) To establish economic screening and quality assurance procedures for shock testing production items and
- (4) To assess the shock survivability of proposed structural designs.

Two approaches that can be made to these problems are

- (1) To empirically duplicate exactly the shock environment by duplicating the pulse shape, force amplitude and time duration and
- (2) To empirically duplicate the severity of the environment by dissimilar pulses whose severity has been analytically determined to be relatively the same in the frequency response regime of the test item.

The latter method has been used successfully by scientists at BRL since the late sixties for various projects. This technique is dependent on the ability to determine the shock spectra from Duhamel's integral for the test and environmental pulses, thus forming a basis for comparison of severity. The main advantage of the approach is that it permits greater latitude in test facilities and provides a means of comparing different testing systems. It also provides the designer with information concerning the severity of the environment and its effect upon the structure's components.

Justification for the method is proven by consideration of several aspects of the behavior of structures. First, all structural systems are complex oscillators and they have responses in specific frequency regimes unique to the particular systems. Therefore, tests to determine survivability need only reflect the energy and momentum existing in the frequency regimes of interest.

Secondly, the relative response of the structure is deterministic and repeatable for any given pulse shape.

Thirdly, the response of the structure can be described by two spectra: the first being the primary spectrum showing the forced vibration response during the time duration of the pulse; the second being the residual spectrum showing the free vibration response after the pulse.

II. BASIC EQUATION FOR DUHAMEL'S INTEGRAL

The spectra are obtained by calculating the response of systems with discrete frequencies using the Duhamel integral over a time period three times the pulse duration. The integral in the form used is shown in Eq. (1).

$$A_r = \left[x_0 \omega_n^2 - \frac{1}{\omega_n} \int_0^s A(t_v) \sin(\omega_n t_v) dt_v \right] \cos(\omega_n s) + \left[\dot{x}_0 \omega_n + \frac{1}{\omega_n} \int_0^s A(t_v) \cos(\omega_n t_v) dt_v \right] \sin(\omega_n s) \quad (1)$$

where A_r = response acceleration

x_0 = initial displacement of the system

\dot{x}_0 = initial velocity of the system

ω_n = natural frequency of the system

$A(t_v)$ = instantaneous acceleration of the pulse at time t_v

t_v = time of observation

s = period of the system of frequency ω_n .

A numerical approach was necessary because the parameter that describes the motion ($A(t_v)$) is generally an unknown function that is approximated by a set of ordered pairs taken from a digitized set of experimental firing data.

If we assume that the pulse starts with zero displacement and velocity, then Eq. (1) can be simplified to that shown in Eq. (2).

$$A_r = \frac{\sin(\omega_n s)}{\omega_n} \int_0^s A(t_v) \cos(\omega_n t_v) dt_v - \frac{\cos(\omega_n s)}{\omega_n} \int_0^s A(t_v) \sin(\omega_n t_v) dt_v \quad (2)$$

Since the sum of the integral equals the integral of the sum, Eq. (2) can be expanded so that we do not integrate from zero for each point of the time history. The natural frequency ω_n of the system in Eq. (3) is replaced by the damped frequency ω_d . This damped frequency is calculated by multiplying the natural frequency by $\sqrt{1-\delta^2}$, where δ is the damping factor. The expanded Eq. (2) with the damped frequency is shown in Eq. (3).

$$A_{r_{i+1}} = \frac{1}{\omega_\delta} \left[\sin(\omega_\delta t_{i+1}) \left\{ \int_{s_0}^{s_i} A(t_v) \cos(\omega_\delta t_v) dt_v + \int_{s_i}^{s_{i+1}} A(t_v) \cos(\omega_\delta t_v) dt_v \right\} \right. \\ \left. - \cos(\omega_\delta t_{i+1}) \left\{ \int_{s_0}^{s_i} A(t_v) \sin(\omega_\delta t_v) dt_v + \int_{s_i}^{s_{i+1}} A(t_v) \sin(\omega_\delta t_v) dt_v \right\} \right] \quad (3)$$

Because it is not necessary to integrate from zero for each point of time history, Eq. (3) provides considerable savings in central processing unit (cpu) time. Hence, Eq. (3) was used in the program instead of Eq. (2). This equation produces the primary system response for a given frequency.

A damping coefficient, which takes into account the viscous loss due to velocity in the system, has been incorporated into Eq. (3). This coefficient was determined from Eq. (4).

$$Damp_p = e^{(-\delta \omega_n s)} \quad (4)$$

where $Damp_p$ = damping coefficient for primary system response

δ = damping factor

ω_n = natural frequency of the system

s = period of the system of frequency ω_n .

The residual system response is obtained analytically from Eq. (5).

$$R_t = Ar_z \cos(\omega_\delta(t-z)) + A'r_z \sin(\omega_\delta(t-z)) \quad (5)$$

where R_t = residual response acceleration at time z

Ar_z = response acceleration at time z

$A'r_z$ = response velocity at time z

t = time after pulse ends

ω_δ = damped frequency of the system

z = pulse duration.

As in the primary system response, the natural frequency in Eq. (5) has been replaced by a damped frequency. Eq. (6) shows the resulting formulation.

$$R'_t = Ar_z e^{(-\delta\omega_d(t-z))} \cos(\omega_d(t-z)) + \frac{A'r_z e^{(-\delta\omega_d(t-z))}}{\omega_d} \sin(\omega_d(t-z)) \quad (6)$$

Where the definitions of all variables are the same as those previously listed in Eqs. (4) and (5).

III. THE COMPUTER PROGRAM

The BRL mainframe computer during the past few years has been a Control Data Corporation (CDC) CYBER 7600(MFZ). The two front-end machines were a CYBER 750(MFA) and an 825(MFB). Two new BRL supercomputers, the CRAY XMP/48 and the CRAY 2 have been installed at the BRL site. There are various minicomputers and microcomputers within the divisions of BRL. The IBD has several Hewlett-Packard (HP) microcomputers, namely the HP9845C, the HP9836C and the HP9000. Also, within the IBD is an HP1000F minicomputer.

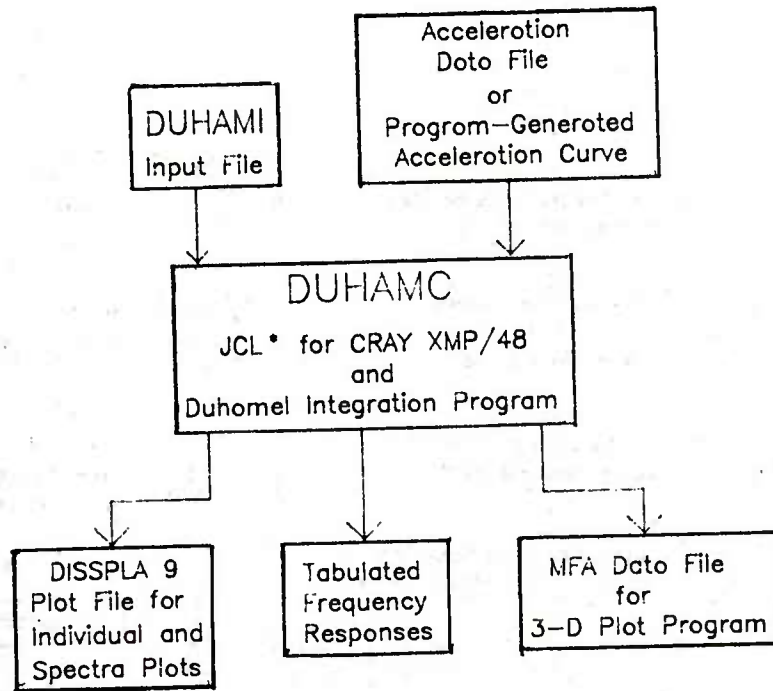
A computer program was written to numerically evaluate Duhamel's integral. The numerical integration scheme used in this program is Simpson's integration. The reciprocal of a given frequency is used as the period of the function. Additionally, the step size for Simpson's integration is less than one-eighth the period to attain reasonable accuracy using this numerical integration scheme. This step size scheme was selected so that the program would use fewer calculations in the lower frequencies.

The natural frequency ω of the system, given by $\omega = 2\pi f$ where f is the inputted frequency (in Hertz), is an integral part of the function being integrated as illustrated in Eqs. (1) through (6).

The Duhamel integral is currently coded in both FORTRAN and BASIC programming languages and has been run on the Hewlett-Packard (HP) 9845C, 9836C, CYBER 750, 825 and 7600 and the CRAY XMP/48. The code can also be used on the HP1000, HP9000 and other machines which support FORTRAN and/or BASIC. The FORTRAN version is currently being prepared, along with its job control language, to be run on the CRAY 2 machine.

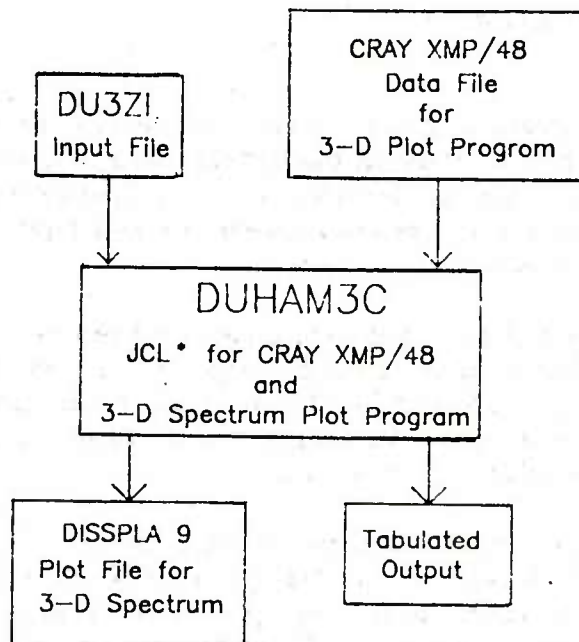
The program is fully documented and is generic for both damped and undamped systems. The FORTRAN code along with its associated job control language for CRAY XMP/48 is listed in Appendix A.

The functions and interrelationships of files run on CRAY XMP/48 are found in Figures 1 and 2. Figure 3 is a general flow diagram of the basic program.



* Job Control Language

Figure 1. CRAY XMP/48 Integration Program Sequence



* Job Control Language

Figure 2. CRAY XMP/48 3-D Plot Program Sequence

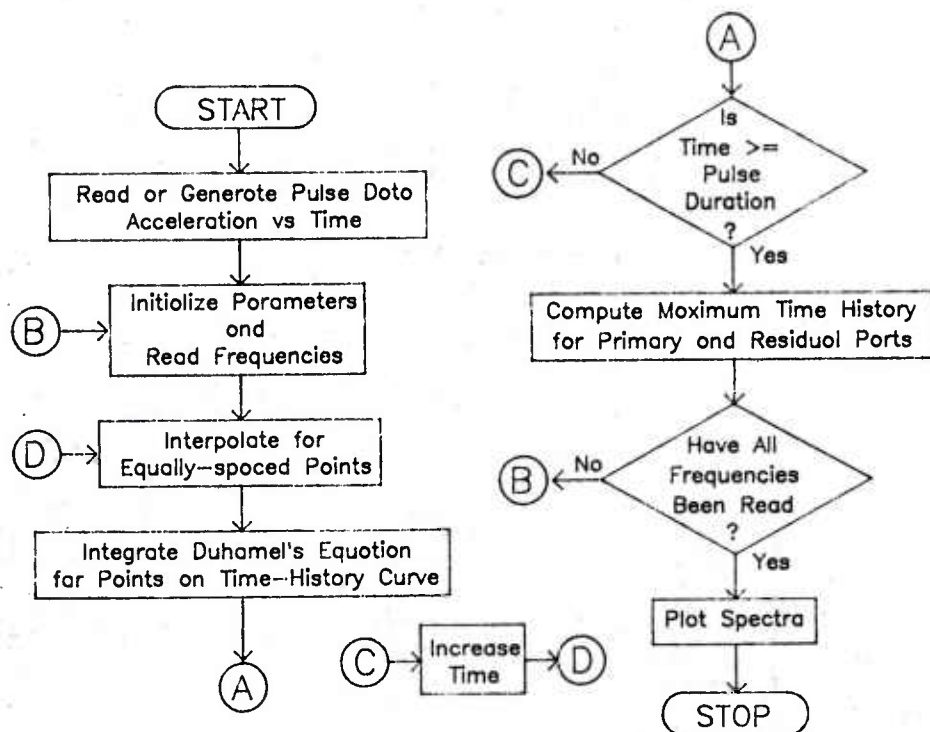


Figure 3. General Flow Diagram of the Basic Integration Program

A. Input to the Computer Program

The first step in establishing test criteria is to obtain response spectra of the shock pulse representing the environment. Thus far, the half-sine pulse, test machine pulses, interior ballistic pulses, idealized free-space blast, modified free-space blast and measured confined blast pulses have been used as representations of the environment. Figures 4 through 8 are examples of these different types of shock pulses.

These types of shock pulses are used as input to the program. Figure 4, a half-sine pulse, is an example of a code-generated curve which was generated in the Duhamel code. The idealized free-space blast and modified blast pulses, Figures 5 and 6, are curves that were generated in an auxiliary program for utilization in the Duhamel code. Figures 7 and 8 are examples of actual experimental data curves taken from firing data.

The amplitude of the input data curves is normalized to one, thus eliminating the need for dimensions. The frequency axis is normalized by multiplying the frequency by the pulse duration. This yields cycles. Depending on the program option selected, the frequency characteristics can be inputted from the keyboard, read from the data statement within the program or included as a part of the input file. The frequency range is generally between .1 and 10000 cycles. The damping characteristics are inputted from the keyboard or from a data file and range from zero to one. Figure 9 is an example of input data. Table 1 defines the input variables and lists the formats.

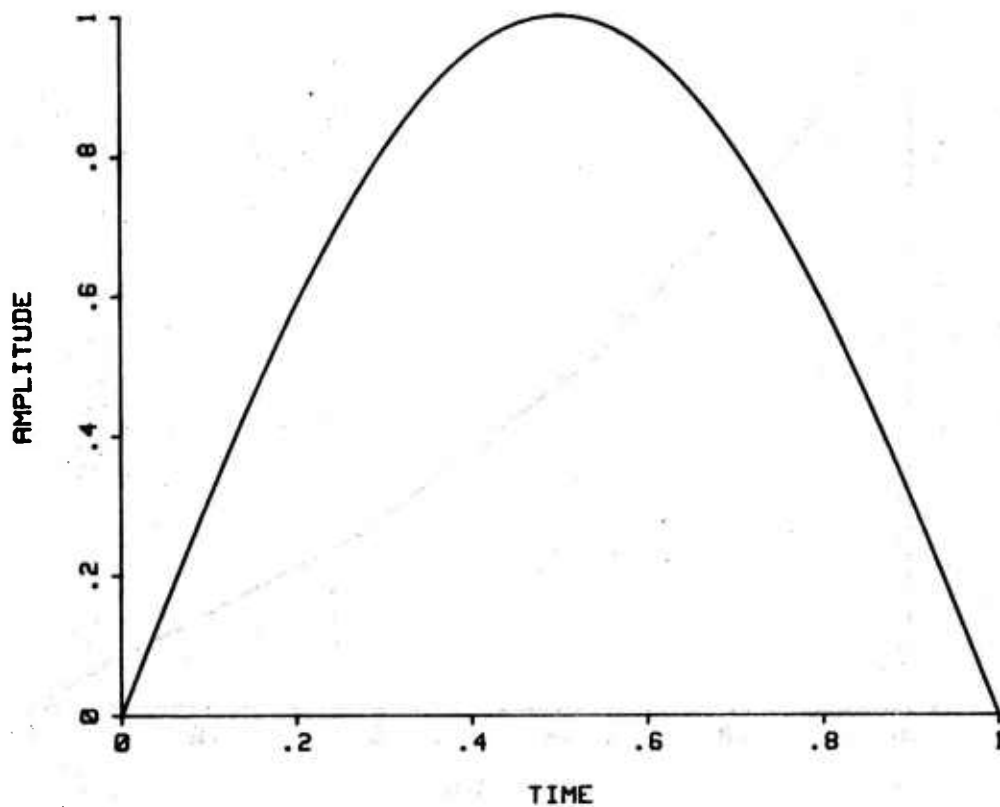


Figure 4. Program Input - Half-Sine Pulse

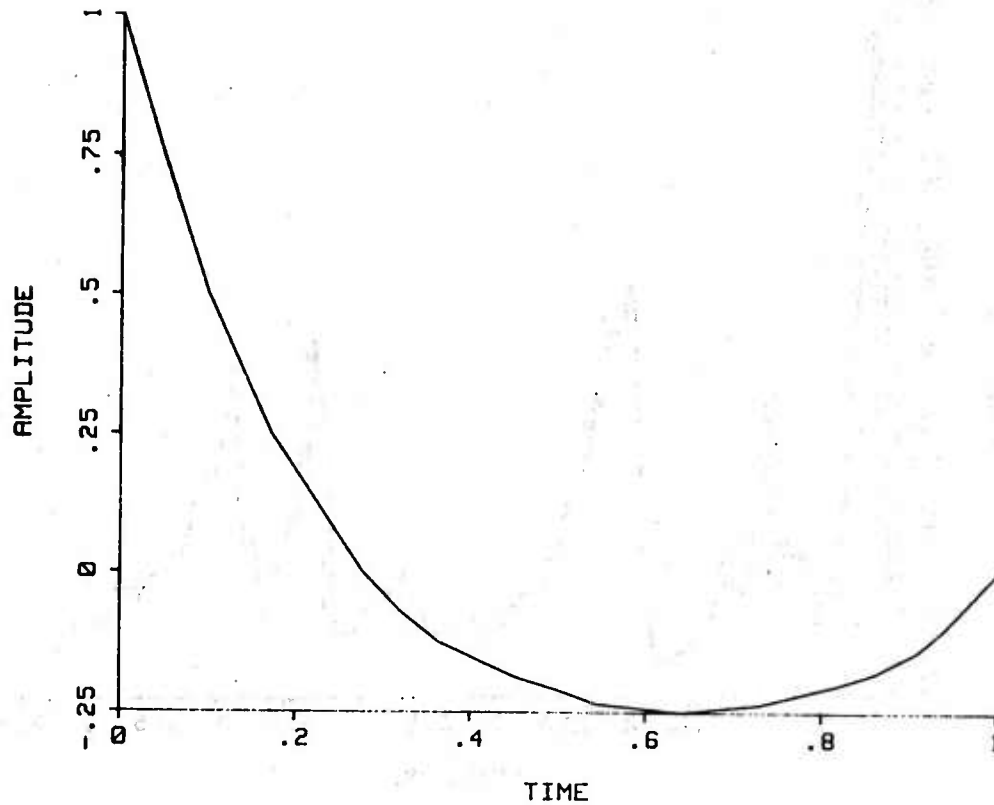


Figure 5. Program Input - Idealized Free-Space Blast Pulse

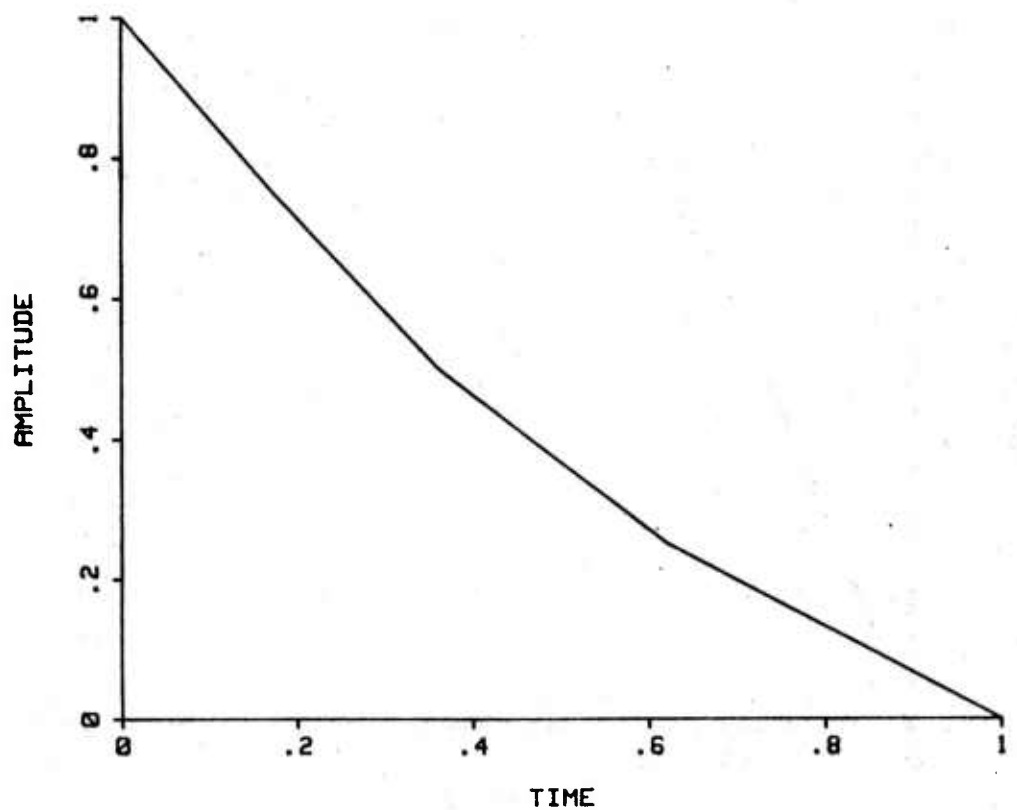


Figure 6. Program Input - Modified Blast Pulse (Positive Portion)

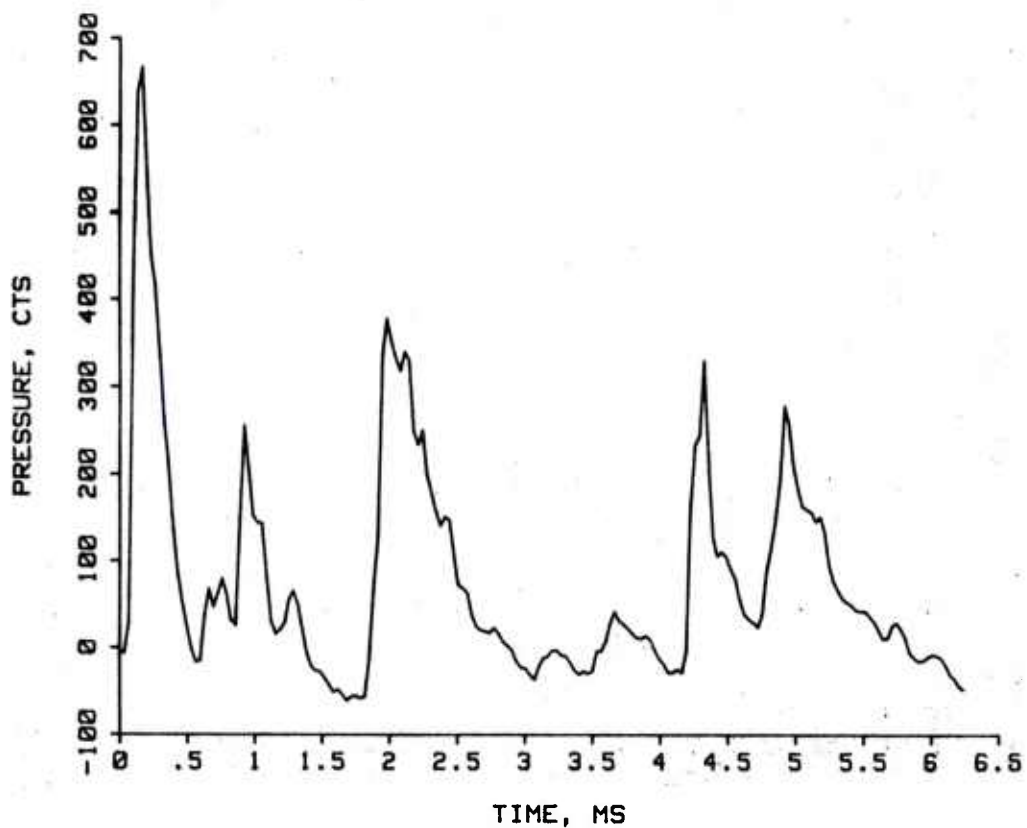


Figure 7. Program Input - Pressure Pulse Tera Socorro ID 24

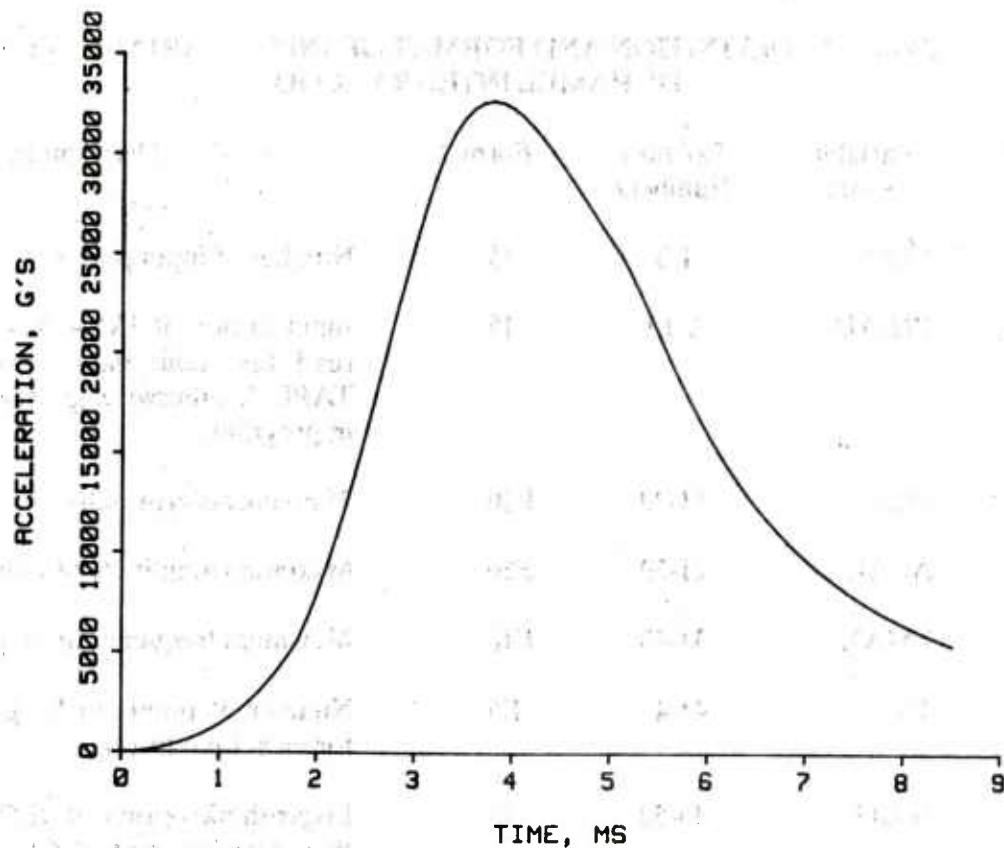


Figure 8. Program Input - Acceleration Pulse 105-mm Gun M68 M456A2

Card Number	Data
1	201 0 3.14159 1.0 10000.100. 0 1 1 1 0
2	105MM GUN, M68 M456A2
3	ACC-TIME HISTORY OF M456A2
4	TIME, MSEC ACCELERATION, G'S
7a	.000
10	SHOCK SPECTRA M456A2
11	FRQ * PULSE DURATION STATIC ACCELERATION
12	.1 10000.0 1000. 0.0 5.0 1.

Figure 9. Sample FORTRAN Card Image Input For Duhamel Integral Code

**TABLE 1. DEFINITION AND FORMAT OF INPUT VARIABLES TO
DUHAMEL INTEGRAL CODE**

Record Number	Variable Name	Column Numbers	Format	Description
1	NOC	1-5	I5	Number of input points.
	IREAD	6-10	I5	Input option, if IREAD = 1, then read the input data curves from TAPE 1, otherwise, generate curve in program.
	TCAL	11-20	F10	Time duration of pulse.
	ACAL	21-30	F10	Maximum amplitude of input pulse.
	FMAX	31-40	F10	Maximum frequency times pulse duration.
	TS	41-45	F5	Number of points to be generated for each time history.
	ILOG	46-50	I5	Logarithmic option, if ILOG = 1, then calculate and plot logarithmic values of frequency.
	IRES	51-55	I5	Residual option, if IRES = 1, then plot only residual spectrum.
	IFREQ	56-60	I5	Frequency option, if IFREQ = 1, then convert frequency times pulse duration to frequency.
	ISPEC	61-65	I5	Spectra option, if ISPEC = 1, then plot both primary and residual spectra.
	I3D	66-70	I5	3-D option, if I3D = 1, then plot a 3-D spectra surface.
	IPLOR	71-72	I2	Plot option, if IPLOR = 1, then plot the original input pulse, unnormalized.
	IPLNO	73-74	I2	Plot option, if IPLNO = 1, then plot the original input pulse, normalized.

TABLE 1. DEFINITION AND FORMAT OF INPUT VARIABLES TO
DUHAMEL INTEGRAL CODE(cont.)

Record Number	Variable Name	Column Numbers	Format	Description
2	PGTIT	1-80	10A8	Page title to be printed on tabulated output.
3	TIT4	1-80	10A8	Plot title for unnormalized input pulse.
4	LXNAME	1-24	3A8	Label for x axis for plot of unnormalized input pulse.
	LYNAME	25-48	3A8	Label for y axis for plot of unnormalized input pulse.
5	TIT4	1-80	10A8	Plot title for normalized pulse.
6	LXNAME	1-24	3A8	Label for x axis for plot of normalized input pulse.
	LYNAME	25-48	3A8	Label for y axis for plot of normalized input pulse.
7	FT	1-10	F10	Frequency times pulse duration.
	DAMP	11-20	F10	Damping characteristic.
	IPLOT	21-25	I5	Plot option, if IPLOT = 1, then plot the time history of the individual frequency.
7a	DAMP	1-10	F10	If a spectra is being plotted, then the damping characteristic is the only variable on Input Card 7 that needs to be read. It only needs to be read once, not for each frequency.
8	TIT4	1-80	10A8	Plot title for plot of time history of an individual frequency.
9	LXNAME	1-24	3A8	Label for x axis for plot of time history of an individual frequency.

**TABLE 1. DEFINITION AND FORMAT OF INPUT VARIABLES TO
DUHAMEL INTEGRAL CODE(cont.)**

Record Number	Variable Name	Column Numbers	Format	Description
9	LYNAME	25-48	3A8	Label for y axis for plot of time history of an individual frequency.
10	TIT4	1-80	10A8	Plot title for plot of residual and/or primary spectra.
11	LXNAME	1-24	3A8	Label for x axis for plot of residual and/or primary spectra.
	LYNAME	25-48	3A8	Label for y axis for plot of residual and/or primary spectra.
12	XORIG	1-10	E10.3	Minimum x-scale value for plot of residual and/or primary spectra.
	XMAX	11-20	E10.3	Maximum x-scale value for plot of residual and/or primary spectra.
	XSTP	21-30	E10.3	Data units per x-scale plot inch for plot of residual and/or primary spectra.
	YORIG	31-40	E10.3	Minimum y-scale value for plot of residual and/or primary spectra.
	YMAX	41-50	E10.3	Maximum y-scale value for plot of residual and/or primary spectra.
	YSTP	51-60	E10.3	Data units per y-scale plot inch for plot of residual and/or primary spectra.

B. Output From the Computer Program

Two spectra are obtained as output from the Duhamel code.

The primary spectrum which is the maximum positive or negative relative acceleration achieved during the pulse.

The residual spectrum which is the maximum positive or negative relative acceleration achieved after the pulse.

Both spectra are plotted versus frequency.

The tabulated output of the Duhamel code includes the input in its original form, the input in its normalized form and the individual responses for the selected frequencies.

The plotted output is a choice of any or all of the following:

- (a) the input curve in original form,
- (b) the input curve in normalized form,
- (c) individual frequency response,
- (d) a spectra of the primary and residual system responses to the given frequencies, and/or
- (e) a three-dimensional mapping of the primary and residual system responses showing relative acceleration, time and frequencies.

C. Plot Routines

On the Hewlett-Packard machines, there is a separate plot routine for each of the plot options. The data are stored on disc and then read in by the selected plot program. In the case of the 3-D option, on all of the machines, the data must be stored for each system response individually. The data are then read by the 3-D routine, geometrically rotated and subsequently plotted. The rotation is done to provide an optimum view of each of the individual system responses. The FORTRAN code for the 3-D plot and the associated job control language for the CRAY XMP/48 are listed in Appendix B. Figure 10 is an example of actual input data while Table 2 provides a listing, including descriptions and formats, of the input variables for the 3-D spectra plot.

On the Hewlett-Packard machines, the HP graphics routines are used, while on the CRAY XMP/48, the graphics are done using the commercial plotting package DISSPLA. Version 9 of DISSPLA is now resident on the CRAY XMP/48. The plots created using DISSPLA can be displayed on a terminal screen, plotted on a printer attached to an interactive terminal and/or transferred to the CALCOMP plotter at the BRL central computer site for hardcopy.

Card Number	Data
1	50 2
2	105MM GUN, M68 M456A2
3	0. 2.5 .3125 -4. 1.5 .9167

Figure 10. Sample FORTRAN Card Image Input for Duhamel 3-D Spectra Plot

**Table 2. DEFINITION AND FORMAT OF INPUT VARIABLES FOR
DUHAMEL 3-D SPECTRA PLOT**

Record Number	Variable Name	Column Numbers	Format	Description
1	NFILES	1-5	I5	Number of response files to be plotted.
	MAXT	6-10	I5	Maximum time of response plot. 1 = Primary response only 2 = Primary and partial residual responses 3 = Primary and full residual responses
2	TIT4	1-80	10A8	Plot title
3	XORIG	1-10	E10.3	Minimum x-scale value
	XMAX	11-20	E10.3	Maximum x-scale value
	XSTP	21-30	E10.3	Data units per x-scale plot inch
	YORIG	31-40	E10.3	Minimum y-scale value
	YMAX	41-50	E10.3	Maximum y-scale value
	YSTP	51-60	E10.3	Data units per y-scale plot inch

Figures 11, 12 and 13 show the response of systems with 30 cycles normalized frequency and .05 damping to the pulses in Figures 5 through 7, respectively. Figures 11 through 13 are individual system responses versus time for a single frequency. Figure 14 is an overlay of Figures 11, 12 and 13.

Figure 15 is the response spectra of systems with .1 to 10000 cycles normalized frequencies and .05 damping applied to the half-sine pulse, Figure 6. Figures 16 through 20 are response spectra of systems with .1 to 10000 cycles normalized frequencies and no damping applied to Figures 4 through 8, respectively. Figures 11 through 14 show both primary and residual response spectra versus frequency plotted on a semi-log plot.

In actuality, these represent normalized response curves where the abscissa is frequency times pulse duration (cycles) and the ordinate is in relative acceleration (dimensionless).

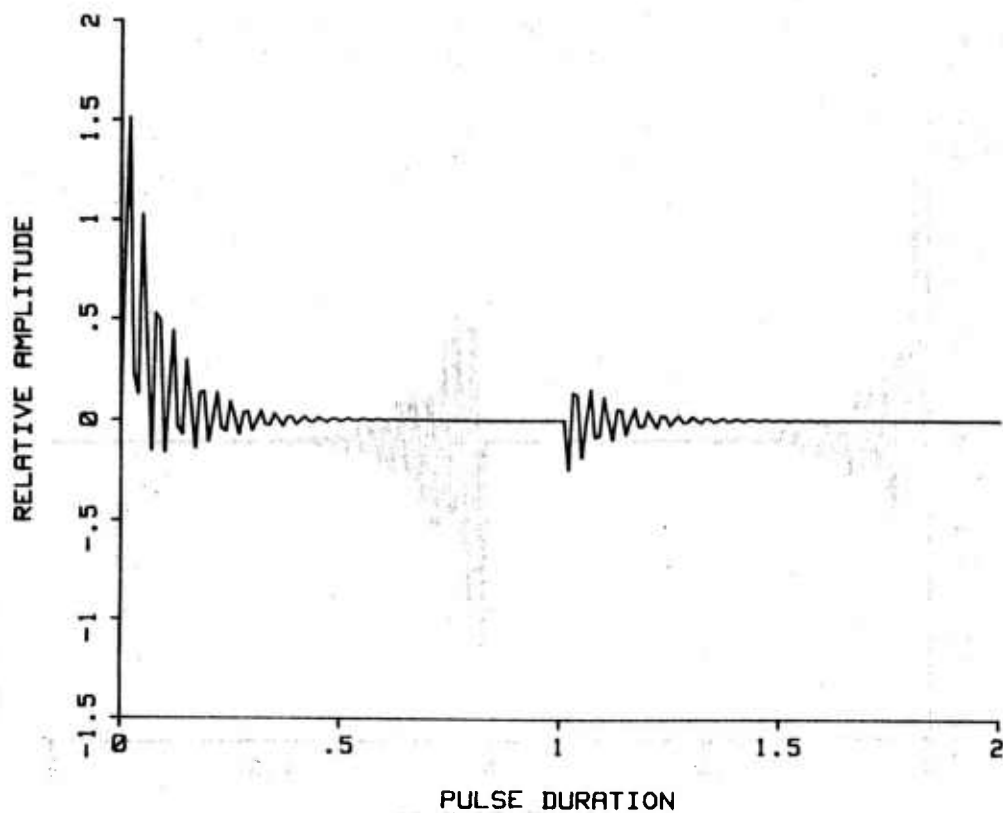


Figure 11. Response Curve (Frequency=30, Damping=.05) Idealized Free-Space Blast Pulse

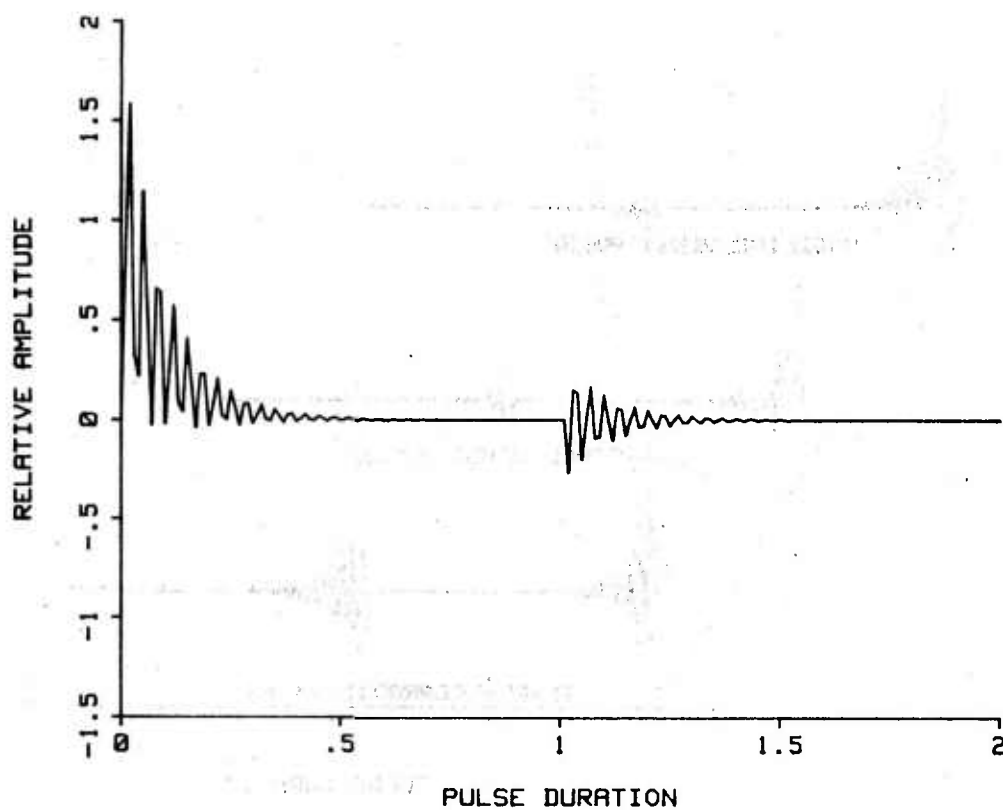


Figure 12. Response Curve (Frequency=30, Damping=.05) Modified Blast Pulse (Positive Portion)

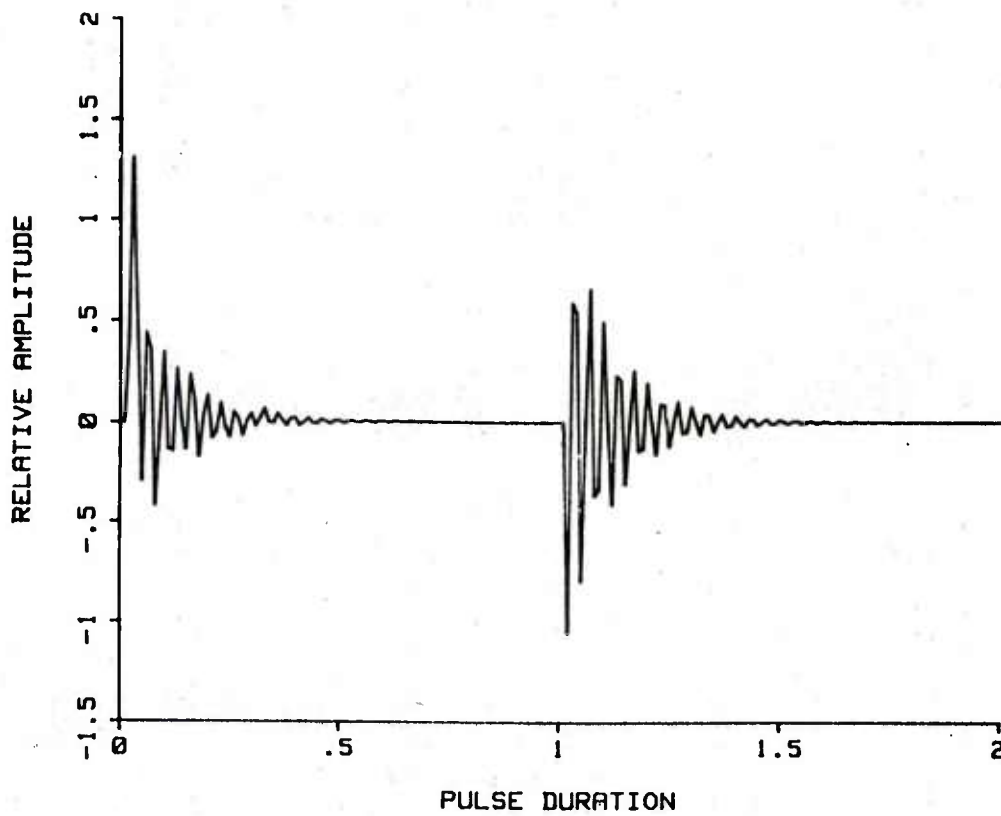


Figure 13. Response Curve (Frequency=30, Damping=.05) Pressure Pulse
Tera Socorro ID 24

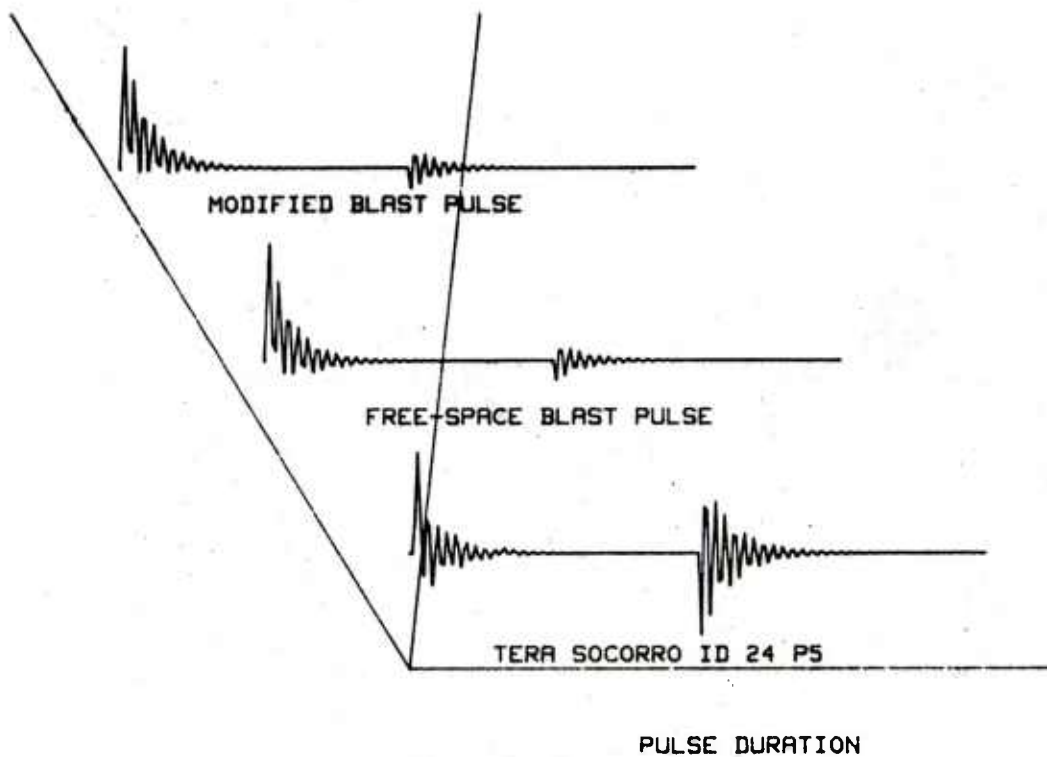


Figure 14. Comparison Response Curves (Frequency=30, Damping=.05)

NORMALIZED SHOCK RESPONSE SPECTRA

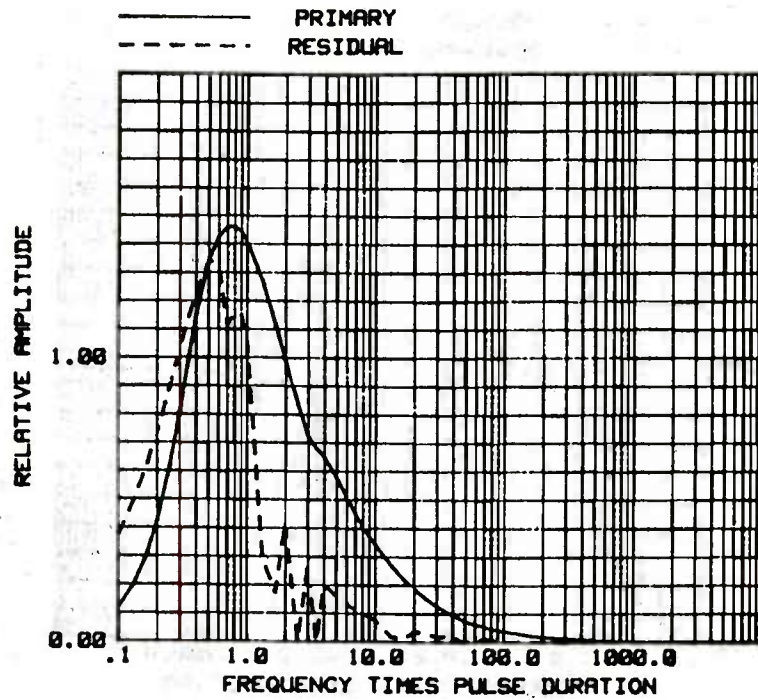


Figure 15. Normalized Shock Response Spectra - Half-Sine Pulse (Damping = .05)

NORMALIZED SHOCK RESPONSE SPECTRA

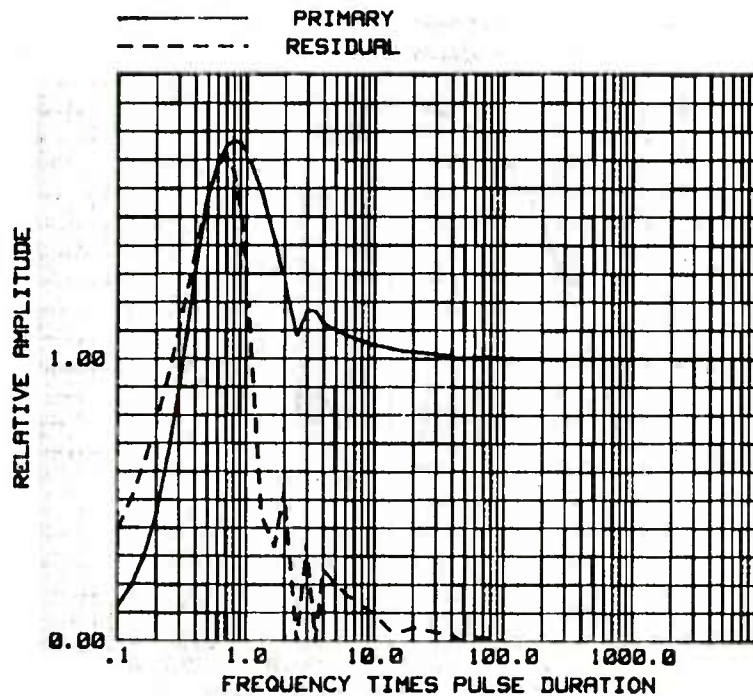


Figure 16. Normalized Shock Response Spectra - Half-Sine Pulse (Undamped)

NORMALIZED SHOCK RESPONSE SPECTRA

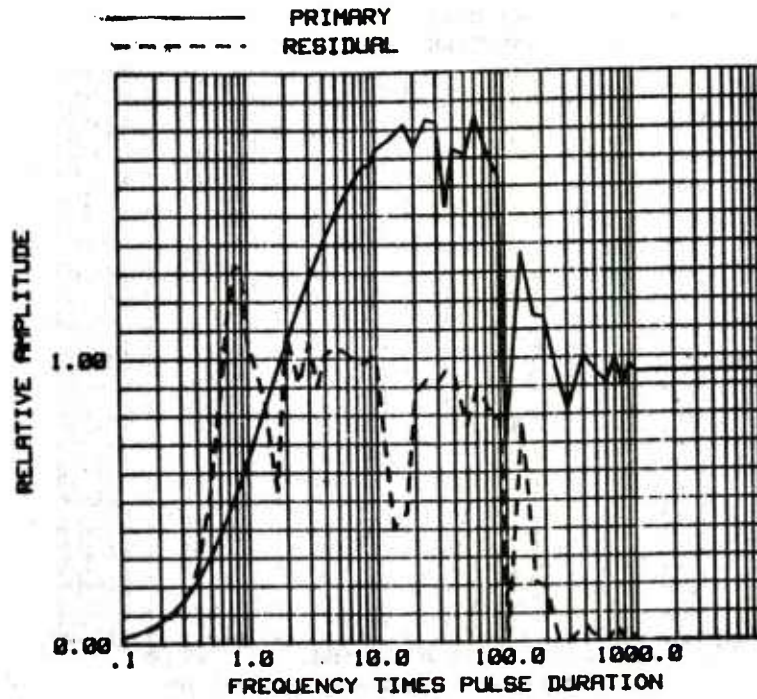


Figure 17. Normalized Shock Response Spectra - Idealized Free-Space Blast Pulse

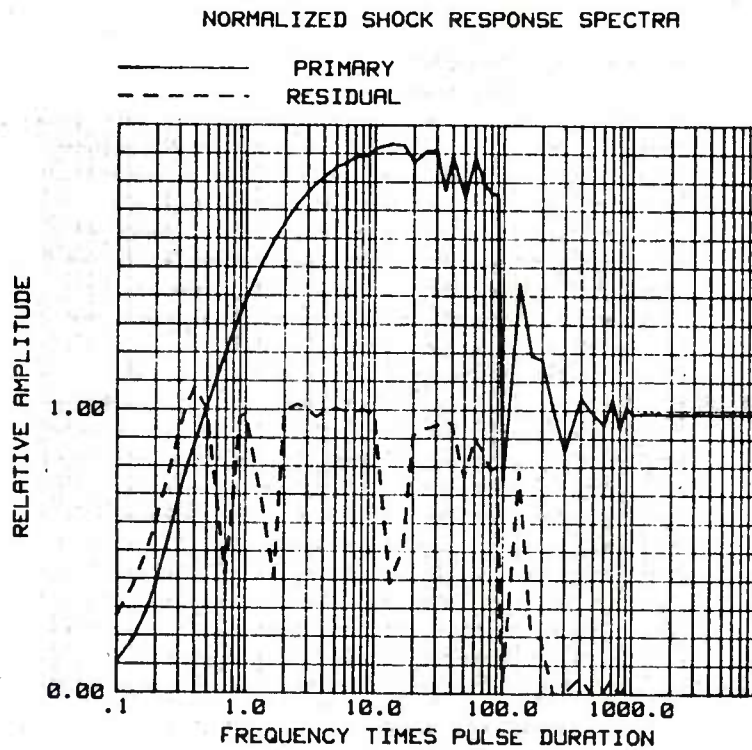


Figure 18. Normalized Shock Response Spectra - Modified Blast Pulse (Positive Portion)

NORMALIZED SHOCK RESPONSE SPECTRA

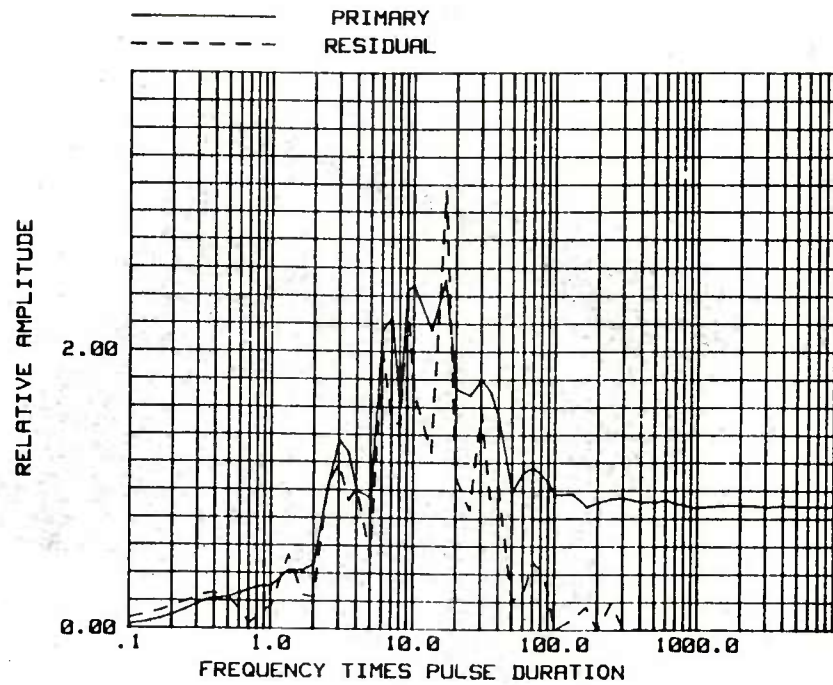


Figure 19. Normalized Shock Response Spectra - Pressure Pulse
Tera Socorro ID 24

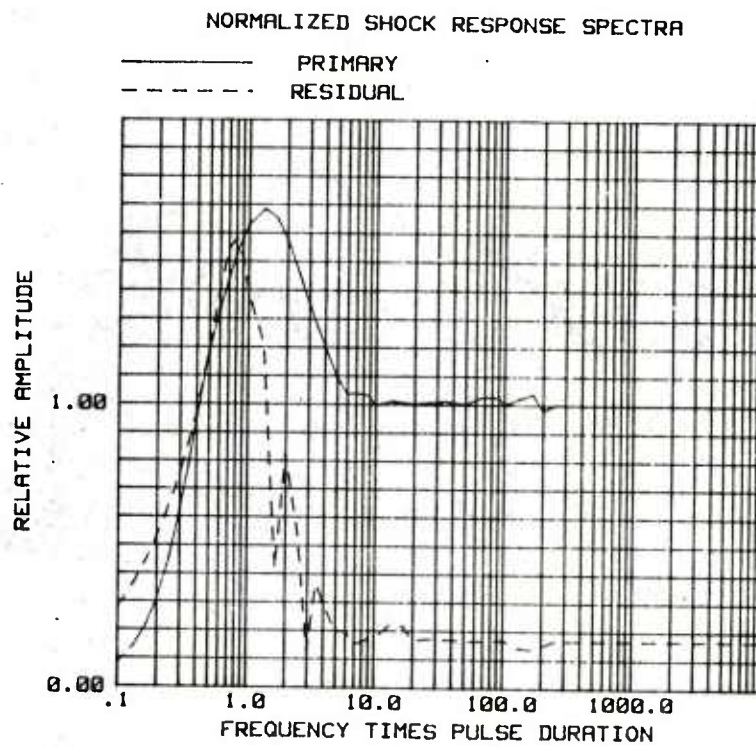


Figure 20. Normalized Shock Response Spectra - Acceleration Pulse
105-mm Gun M68 M456A2

Figures 21 through 26 are 3-D mappings of the response spectra shown in Figures 15 through 20, respectively. The three dimensions are relative acceleration, time and frequency.

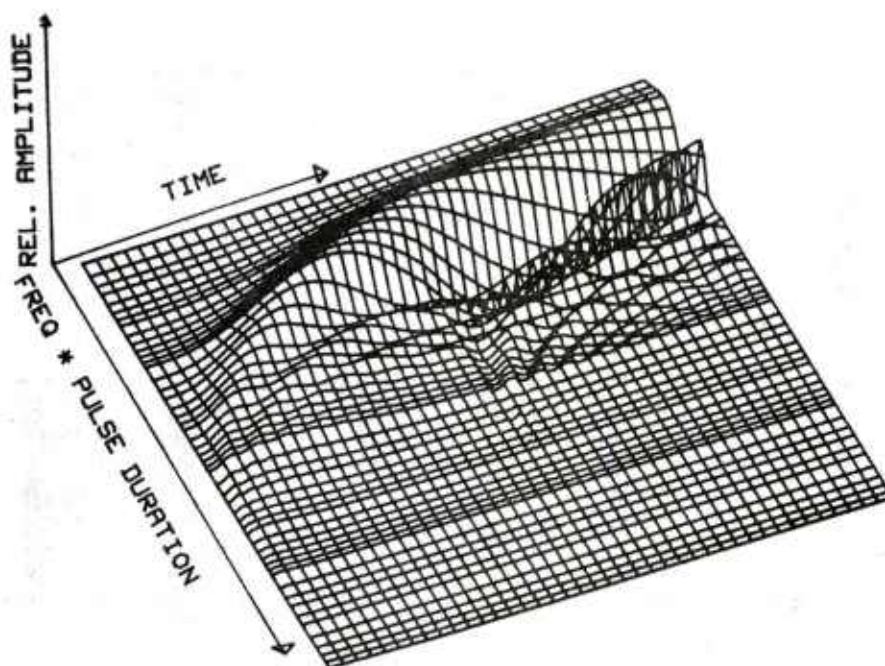


Figure 21. 3-D Shock Response - Half-Sine Pulse (Damping = .05)

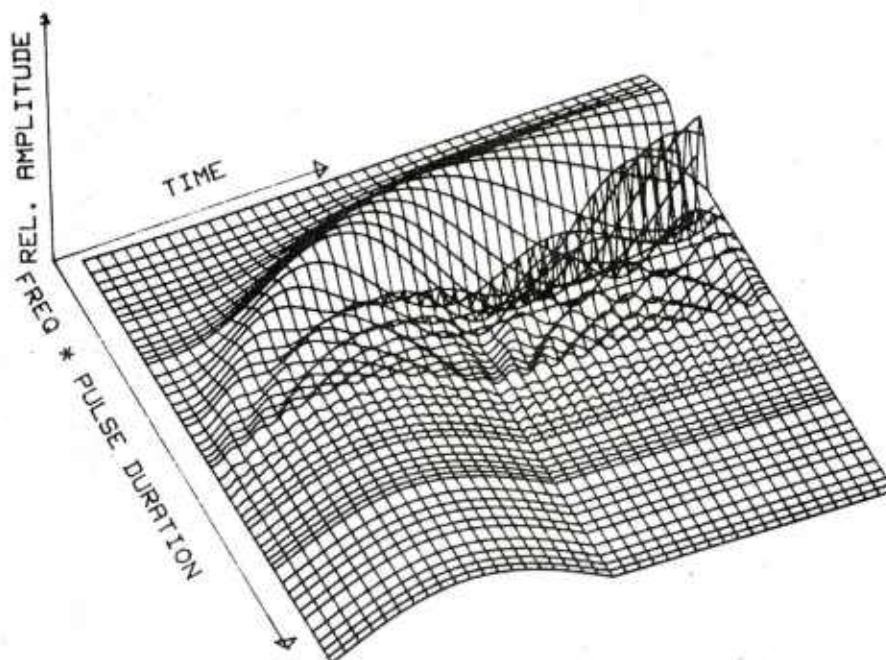


Figure 22. 3-D Shock Response - Half-Sine Pulse (Undamped)

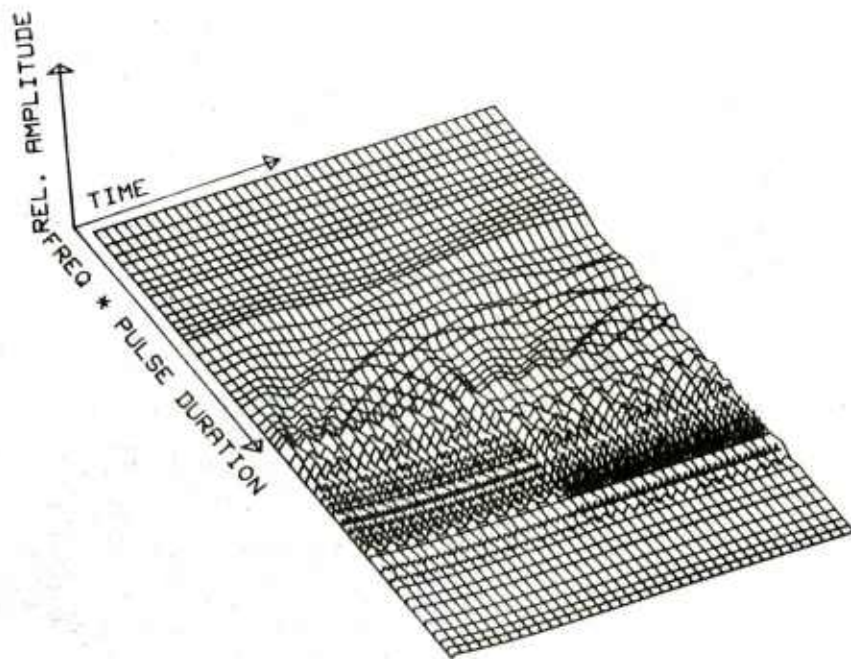


Figure 23. 3-D Shock Response - Idealized Free-Space Blast Pulse

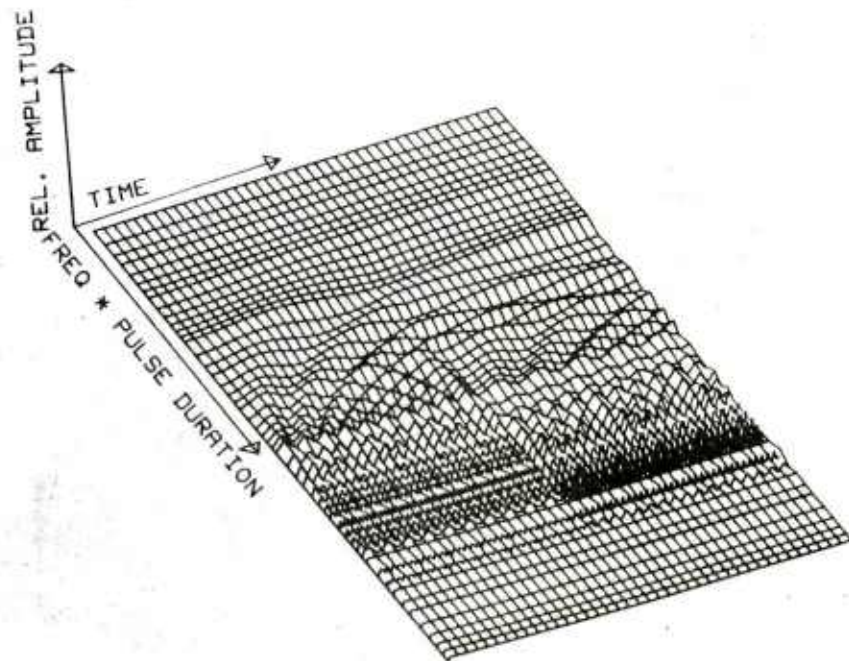


Figure 24. 3-D Shock Response - Modified Blast Pulse (Positive Portion)

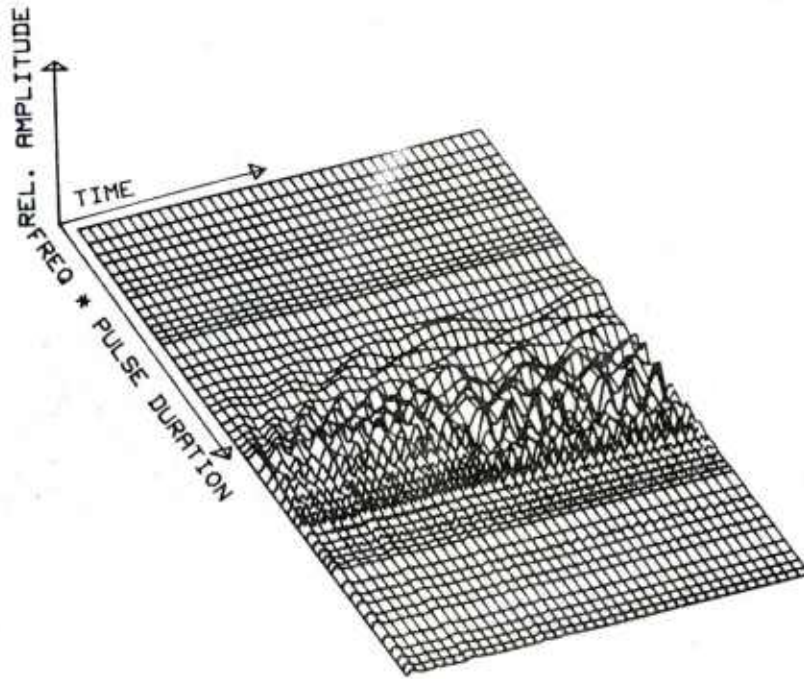


Figure 25. 3-D Shock Response - Pressure Pulse Tera Socorro ID 24

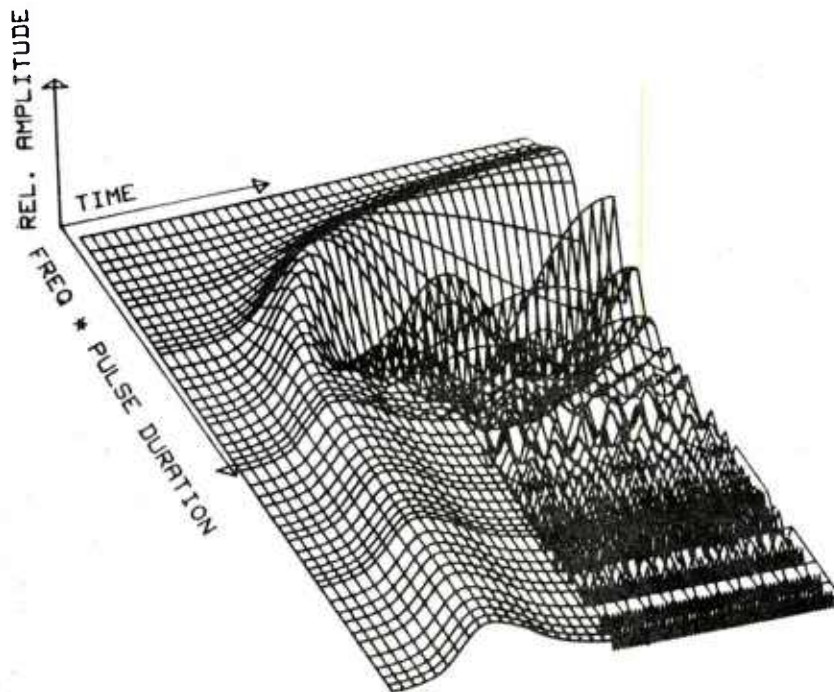


Figure 26. 3-D Shock Response - Acceleration Pulse 105-mm Gun M68 M456A2

IV. SUMMARY

The Duhamel's integral computer code was developed to analyze the transient response of test instrumentation and structures and to assess damage to the human ear caused by nonclassical pressure pulses. The code has been used to assess the relative severity of laboratory test environments with respect to gun environments. The program has been installed on a mainframe, a front-end machine and several microcomputers in BASIC and FORTRAN programming languages so as to make it more accessible to the user.

The Duhamel's integral package is now being run on the CRAY 2 supercomputer which, along with the CRAY XMP/48, has replaced the CYBER 7600 at the BRL. This code will be incorporated into the general structural and analysis scheme of the IBD. In addition, the program will be extended to compound response descriptions which include more than one frequency and other nonlinear forms, such as hardening and softening stiffness systems.

APPENDIX A

LISTING OF FORTRAN PROGRAM TO INTEGRATE DUHAMEL'S INTEGRAL
ALONG WITH ASSOCIATED JOB CONTROL LANGUAGE FOR CRAY XMP/48

APPENDIX A

LISTING OF FORTRAN PROGRAMS TO INTEGRATE DUHAMEL'S INTEGRAL ALONG WITH ASSOCIATED JOB CONTROL LANGUAGE FOR CRAY XMP/48

I. Job Control Language for CRAY XMP/48

```
JOB,JN=jobname,T=150,MFL=350000.  
ACCOUNT,AC=accountnumber,US=username,UPW=userpassword.  
ACCESS,DN=DISLIB,PDN=DISLIB,ID=DISSPLA,OWN=SYSTEM.  
ACCESS,DN=DVSD,PDN=DVSD,ID=DISSPLA,OWN=SYSTEM.  
ACCESS,DN=INTLIB,PDN=INTLIB,ID=DISSPLA,OWN=SYSTEM.  
FETCH,DN=infile,TEXT='CHARGE,acctno,pn.GET,infile=infile.CTASK.'
```

where *infile* = name of input file which contains program options
and plot titles
pn = first two letters of the account number

```
ASSIGN,DN=infile,A=FT03.  
FETCH,DN=acfile,TEXT='CHARGE,acctno,pn.GET,acfile=acfile.CTASK.'
```

where *acfile* = name of permanent file residing on front end which
contains data to be used as shock pulse

```
ASSIGN,DN=acfile,A=FT01.  
ASSIGN,DN=TAPE2,A=FT02.  
CFT.  
SEGLDR,CMD='LIB=DISLIB,INTLIB',GO.  
DISPOSE,DN=META,DC=ST,DF=BB,^  
TEXT='CHARGE=acctno,pn.CTASK.REPLACE,META=pfm.'
```

where *pfm* = name of output file in which the DISSPLA plot file
is stored on the front end.

```
DISPOSE,DN=TAPE2,DC=ST,DF=BB,^  
TEXT='CHARGE=acctno,pn.CTASK.REPLACE,TAPE2=3dfile.'
```

where *3dfile* = name of output file that will contain data to
be used in calculations for 3-D plot.

II. Listing of FORTRAN File

	PROGRAM SPECTRM(INPUT,OUTPUT,TAPE1,TAPE5,TAPE6=OUTPUT,	SPEC 1
	*META,TAPE10=OUTPUT,TAPE2)	SPEC 2
C	THIS PROGRAM NUMERICALLY INTEGRATES DUHAMEL'S INTEGRAL TO	SPEC 3
C	OBTAIN A PRIMARY AND RESIDUAL SHOCK SPECTRA. THE INPUT	SPEC 4
C	CONSISTS OF A SET OF ORDERED PAIRS THAT DESCRIBE THE	SPEC 5
C	ACCELERATION OF A SYSTEM AND A SET OF FREQUENCIES OVER	SPEC 6
C	WHICH THE SYSTEM IS TO BE EVALUATED. THIS PROGRAM WILL ALSO	SPEC 7
C	PLOT THE PRIMARY AND RESIDUAL SHOCK TIME HISTORY OF A GIVEN	SPEC 8
C	FREQUENCY.	SPEC 9
C		SPEC 10
	DIMENSION RMAX(500),FWN(500),FR(500),MSAVE(75),XPLT(7000)	SPEC 11
	DIMENSION PFT(200),PXP(200),PXR(200),PGTIT(10),YPLT(7000)	SPEC 12
	DIMENSION XA(3500),XB(3500),TA(3500),TB(3500),TIT4(4)	SPEC 13
	DIMENSION U(210),A(210),V(1040),VP(1040),DUM(1),FTR(61)	SPEC 14
	REAL NX, NXP, MAXP, MAXR	SPEC 15
C		SPEC 16
	DATA PI2,PI/6.283185307,3.14159265358/	SPEC 17
C		SPEC 18
C	FREQUENCY INPUT DATA	SPEC 19
C		SPEC 20
	DATA FTR/.1,133,167,2,25,3,35,4,5,6,7,8,9,1,1.333,	SPEC 21
	*1.667,2,2.5,3,3.5,4,5,6,7,8,9,10,13.333,16.667,20,25,	SPEC 22
	*30,35,40,50,60,70,80,90,100,133.333,166.667,200,250,	SPEC 23
	*300,400,500,600,700,800,900,1000,2000,3000,4000,5000,	SPEC 24
	*6000,7000,8000,9000,10000./	SPEC 25
C		SPEC 26
C		SPEC 27
	CALL COMPRS	SPEC 28
	CALL SETDEV(10,6)	SPEC 29
C		SPEC 30
C	ACCELERATION AND TIME ARE NORMALIZED.	SPEC 31
C		SPEC 32
C	NOC = NO. OF INPUT POINTS.	SPEC 33
C	IF IREAD = 1, THEN READ INPUT DATA FROM TAPE1	SPEC 34
C	OTHERWISE, GENERATE DATA IN PROGRAM.	SPEC 35
C	TCAL = TIME DURATION OF PULSE	SPEC 36
C	ACAL = MAXIMUM ACCELERATION OF PULSE	SPEC 37
C	FMAX = MAXIMUM FREQUENCY TIMES PULSE DURATION	SPEC 38
C	TS = THE NUMBER OF POINTS GENERATED FOR EACH TIME HISTORY.	SPEC 39
C	IF ILOG = 1, CALCULATE AND PLOT LOG VALUES OF FREQUENCY	SPEC 40
C	IF IRES = 1, PLOT ONLY RESIDUAL SPECTRUM	SPEC 41
C	IF IFREQ = 1, CONVERT FREQUENCY TIMES PULSE	SPEC 42
C	DURATION TO FREQUENCY.	SPEC 43
C	IF ISPEC = 1, PLOT PRIMARY AND RESIDUAL SPECTRA	SPEC 44
C	IF I3D = 1, PLOT A 3-D SPECTRUM SURFACE.	SPEC 45
C	IF IPLOR = 1, PLOT THE ORIGINAL PULSE, UNNORMALIZED.	SPEC 46
C	IF IPLNO = 1, PLOT THE ORIGINAL PULSE, NORMALIZED.	SPEC 47

C		SPEC 48
C	SET UP PLOT VARIABLES	SPEC 49
C		SPEC 50
	ISC=0	SPEC 51
	ITYPE=0	SPEC 52
	N4=0	SPEC 53
	ICOLOR=0	SPEC 54
	NCURV=1	SPEC 55
C		SPEC 56
C	READ AND PRINT PROGRAM CONTROL VARIABLES	SPEC 57
C		SPEC 58
10	READ(5,1000) NOC,IREAD,TCAL,ACAL,FMAX,TS,ILOG,IRES, *IFREQ,ISPEC,I3D,IPLOR,IPLNO	SPEC 59
	IF(EOF(5).EQ.0.) GO TO 20	SPEC 60
	CALL DONEPL	SPEC 61
	STOP	SPEC 62
20	WRITE(6,1000) NOC,IREAD,TCAL,ACAL,FMAX,TS,ILOG,IRES, *IFREQ,ISPEC,I3D,IPLOR,IPLNO	SPEC 63
		SPEC 64
C		SPEC 65
C	READ IN TITLE AND SET UP OTHER PLOT VARIABLES	SPEC 66
C		SPEC 67
	READ(5,1100) PGTIT	SPEC 68
	WRITE(6,1200) PGTIT	SPEC 69
	IF(IFREQ.EQ.1) FMAX=FMAX/TCAL	SPEC 70
		SPEC 71
C		SPEC 72
C	DO-LOOP TO READ AND NORMALIZE ORDERED PAIRS (U,A)	SPEC 73
C		SPEC 74
	IF(IREAD.NE.1) GO TO 30	SPEC 75
	READ(1,1600) (U(I),A(I),I=1,NOC)	SPEC 76
	GO TO 50	SPEC 77
30	TIME=0.	SPEC 78
	DO 40 I=1,NOC	SPEC 79
	ACC=SIN(TIME)	SPEC 80
	U(I)=TIME	SPEC 81
	A(I)=ACC	SPEC 82
	TIME=TIME+PI/(NOC-1)	SPEC 83
40	CONTINUE	SPEC 84
50	WRITE(6,1300)	SPEC 85
	WRITE(6,1400)	SPEC 86
	WRITE(6,1500) (U(I),A(I),I=1,NOC)	SPEC 87
C		SPEC 88
C	PLOT ORIGINAL INPUT PULSE	SPEC 89
C		SPEC 90
	IF(IPLOR.NE.1) GO TO 60	SPEC 91
	READ(5,1100) TIT4	SPEC 92
	LST=1	SPEC 93
	LSP=NOC	SPEC 94
	CALL DATA4(NCURV,U,A,DUM,NOC,ISC,ITYPE,LST,LSP,TIT4, *ICOLOR)	SPEC 95
	TIME=0.	SPEC 96
		SPEC 97

C		SPEC 98
C	NORMALIZE INPUT PULSE	SPEC 99
C		SPEC 100
60	DO 70 I=1,NOC	SPEC 101
	U(I)=U(I)/TCAL	SPEC 102
	A(I)=A(I)/ACAL	SPEC 103
	UMAX=U(I)	SPEC 104
70	CONTINUE	SPEC 105
C		SPEC 106
C	PRINT NORMALIZED ACCELERATION PULSE	SPEC 107
C		SPEC 108
	WRITE(6,1700)	SPEC 109
	WRITE(6,1300)	SPEC 110
	WRITE(6,1500) (U(I),A(I),I=1,NOC)	SPEC 111
C		SPEC 112
C	PLOT PULSE CURVE	SPEC 113
C		SPEC 114
	IF(IPLNO.NE.1) GO TO 80	SPEC 115
	READ(5,1100) TIT4	SPEC 116
	LST=1	SPEC 117
	LSP=NOC	SPEC 118
	NCURV=1	SPEC 119
	CALL DATA4(NCURV,U,A,DUM,NOC,ISC,ITYPE,LST,LSP,TIT4, *ICOLOR)	SPEC 120
C		SPEC 121
C	TIME AND ACCELERATION MUST START AT 0.	SPEC 122
C		SPEC 123
80	A(1)=0.	SPEC 124
	U(1)=0.	SPEC 125
C		SPEC 126
C	S = RANGE OVER WHICH DUHAMEL'S INTEGRAL IS INTEGRATED	SPEC 127
C	TO OBTAIN A POINT OF TIME HISTORY FOR PRIMARY SHOCK	SPEC 128
C	SPECTRUM. PRIMARY SHOCK SPECTRUM IS GENERATED AS XA VS S.	SPEC 129
C		SPEC 130
	S=0	SPEC 131
C		SPEC 132
C	T IS USED TO GENERATE EQUALLY SPACED POINTS FOR	SPEC 133
C	SIMPSON'S INTEGRATION	SPEC 134
C		SPEC 135
	T=0	SPEC 136
C		SPEC 137
C	DS DETERMINES THE NO. OF POINTS GENERATED FOR EACH	SPEC 138
C	TIME HISTORY.	SPEC 139
C		SPEC 140
	DS=(UMAX-U(1))/TS	SPEC 141
C		SPEC 142
C	NP = NO. OF FREQUENCIES USED	SPEC 143
C		SPEC 144
	NP=1	SPEC 145
C		SPEC 146
		SPEC 147

C	FT IS FREQUENCY TIMES THE PULSE DURATION. F IS FREQUENCY	SPEC 148
C	AND IS EQUAL TO FT SINCE TIME HAS BEEN NORMALIZED.	SPEC 149
C	IF IPLOT EQUALS 1, PLOT TIME HISTORY OF FREQUENCY	SPEC 150
C		SPEC 151
90	IF(IRES.EQ.1.OR.ISPEC.EQ.1.OR.I3D.EQ.1) GO TO 92	SPEC 152
	READ(5,1800) FT,DAMP,IPLOT	SPEC 153
	WRITE(6,1800) FT,DAMP,IPLOT	SPEC 154
	GO TO 94	SPEC 155
92	FT=FTR(NP)	SPEC 156
	IF(NP.EQ.1) READ(5,1800) DAMP	SPEC 157
94	F0=FT	SPEC 158
	FT=FT*SQRT(1.-DAMP**2)	SPEC 159
	F=FT/UMAX	SPEC 160
C		SPEC 161
C	X1 AND X2 ARE RUNNING VALUES OF INTEGRATION AND ARE	SPEC 162
C	SET TO 0 WHEN A NEW FREQUENCY IS READ.	SPEC 163
C		SPEC 164
	X1=0.	SPEC 165
	X2=0.	SPEC 166
	I=1	SPEC 167
	K=1	SPEC 168
	L=1	SPEC 169
	M=1	SPEC 170
C		SPEC 171
C	H IS STEP SIZE FOR SIMPSON'S INTEGRATION	SPEC 172
C		SPEC 173
	H=DS/8.	SPEC 174
C		SPEC 175
C	P = PERIOD OF FUNCTION.	SPEC 176
C		SPEC 177
	P=1./F	SPEC 178
C		SPEC 179
C	H MUST BE LESS THAN 1/8 THE PERIOD FOR REASONABLE	SPEC 180
C	ACCURACY USING SIMPSON'S INTEGRATION.	SPEC 181
C		SPEC 182
100	IF(H.LT.(1./8.)*P) GO TO 110	SPEC 183
	H=H/2.	SPEC 184
	GO TO 100	SPEC 185
110	H3=H/3.	SPEC 186
C		SPEC 187
C	SWS = SIN(WS) AND CWS = COS(WS).	SPEC 188
C		SPEC 189
	W=PI2*F	SPEC 190
	WD=PI2*F0	SPEC 191
120	WS=W*S	SPEC 192
	CWS=COS(WS)	SPEC 193
	SWS=SIN(WS)	SPEC 194
C		SPEC 195
C	U AND A ARE UPDATED FOR PROPER LINEAR INTERPOLATION.	SPEC 196
C		SPEC 197

130	IF(T.GE.U(I).AND.T.LE.U(I+1)) GO TO 150	SPEC 198
	IF(T.LT.UMAX) GO TO 140	SPEC 199
C		SPEC 200
C	T IS SET TO TMAX TO CORRECT POSSIBLE ACCUMULATIVE ERRORS	SPEC 201
C		SPEC 202
	T=UMAX	SPEC 203
	GO TO 150	SPEC 204
140	I=I+1	SPEC 205
	GO TO 130	SPEC 206
C		SPEC 207
C	Y IS THE LINEAR INTERPOLATION F(T). HENCE THE NEW	SPEC 208
C	SET OF EQUALLY SPACED ORDERED PAIRS ARE (T,Y)	SPEC 209
C		SPEC 210
150	Y=(T-U(I))*(A(I+1)-A(I))/(U(I+1)-U(I))+A(I)	SPEC 211
C		SPEC 212
C	WT = 2*PI*F*T SWT = SIN(WT). CWT = COS(WT).	SPEC 213
C		SPEC 214
	WT = W*T	SPEC 215
	SWT=SIN(WT)	SPEC 216
	CWT=COS(WT)	SPEC 217
C		SPEC 218
C	THIS SECTION APPLIES SIMPSON'S INTEGRATION FORMULA TO	SPEC 219
C	ORDERED PAIRS (T,V) AND (T,VP) AND STORES THE RESULTS	SPEC 220
C	IN X AND XP RESPECTIVELY. V AND VP ARE PARTS OF	SPEC 221
C	DUHAMEL'S INTEGRAL THAT ARE TO BE INTEGRATED.	SPEC 222
C		SPEC 223
	V(K)=Y*SWT	SPEC 224
	VP(K)=Y*CWT	SPEC 225
	T=T+H	SPEC 226
	IF(T.LT.0..OR.T.GT.UMAX+H) GO TO 300	SPEC 227
C		SPEC 228
C	T HAS A TOLERANCE H/2 TO ASSURE THAT LAST POINT IS USED.	SPEC 229
C		SPEC 230
	IF(T.GT.S+H/2.) GO TO 160	SPEC 231
	K=K+1	SPEC 232
	GO TO 110	SPEC 233
C		SPEC 234
160	OD=0.	SPEC 235
	EV=0.	SPEC 236
	DO 170 J=2,K,2	SPEC 237
	OD=OD+V(J)	SPEC 238
170	EV=EV+V(J+1)	SPEC 239
	EV=EV-V(K)	SPEC 240
	X=H3*(V(1)+V(K)+4.*OD+2.*EV)	SPEC 241
	OD=0.	SPEC 242
	EV=0.	SPEC 243
	DO 180 J=2,K,2	SPEC 244
	OD=OD+VP(J)	SPEC 245
180	EV=EV+VP(J+1)	SPEC 246
	EV=EV-VP(K)	SPEC 247

	XP=H3*(VP(1)+VP*(K)+4.*OD+2.*EV)	SPEC 248
C		SPEC 249
C	X1 AND X2 SUM TERMS SO THAT WE ARE INTEGRATING OVER	SPEC 250
C	THE RANGE 0. TO S.	SPEC 251
C		SPEC 252
	X1=X1+X	SPEC 253
	X2=X2+XP	SPEC 254
C		SPEC 255
C	NX IS THE INTEGRAL OF DUHAMEL'S EQUATION FOR THE	SPEC 256
C	RANGE 0. TO S.	SPEC 257
C		SPEC 258
	NX=EXP(-DAMP*S*WD)*W*(SWS*X2-CWS*X1)	SPEC 259
	IF (ABS(NX).LT..1E-06) NX=0	SPEC 260
C		SPEC 261
C	(T,NX) IS A POINT ON THE TIME HISTORY CURVE.	SPEC 262
C		SPEC 263
C	WHEN S .LT. UMAX THE PROGRAM INCREASES S BY DS AND	SPEC 264
C	DECREASES T BY H. IT THEN RETURNS TO LOCATION 120	SPEC 265
C	AND BEGINS TO INTEGRATE THE NEXT AREA.	SPEC 266
C		SPEC 267
	IF (S.EQ.0.) GO TO 190	SPEC 268
	I=I-1	SPEC 269
190	T=T-H	SPEC 270
	IF(IRES.EQ.1) GO TO 200	SPEC 271
C		SPEC 272
C	TA STORES T	SPEC 273
C		SPEC 274
	TA(L)=T	SPEC 275
C		SPEC 276
C	XA STORES NX	SPEC 277
C		SPEC 278
	XA(L)=NX	SPEC 279
	XPLT(M)=T	SPEC 280
	YPLT(M)=NX	SPEC 281
	L=L+1	SPEC 282
	M=M+1	SPEC 283
200	K=1	SPEC 284
	IF ((S-UMAX).GE.-.1E-10)GO TO 210	SPEC 285
	S=S+DS	SPEC 286
	GO TO 120	SPEC 287
C		SPEC 288
C	NXP IS THE DERIVATIVE OF THE TIME HISTORY AT UMAX.	SPEC 289
C		SPEC 290
210	ST=W*(T-S)	SPEC 291
	SWST=SIN(ST)	SPEC 292
	CWST=COS(ST)	SPEC 293
	TT=T-S	SPEC 294
	NXP=EXP(-DAMP*WD*TT)*W*W*(X1*SWST+X2*CWST)	SPEC 295
	* +EXP(-DAMP*WD*TT)*W*(DAMP*WD)*(-X2*SWST+X1*CWST)	SPEC 296
C		SPEC 297

C	XMAX IS THE MAXIMUM VALUE OF THE RESIDUAL SPECTRUM	SPEC 298
C		SPEC 299
	$XMAX = \sqrt{NX * NX + NXP * NXP / W / W}$	SPEC 300
C		SPEC 301
	L=1	SPEC 302
220	ST=WD*(T-S)	SPEC 303
	SWST=SIN(ST)	SPEC 304
	CWST=COS(ST)	SPEC 305
	TT=T-S	SPEC 306
C		SPEC 307
C	(TB,XB) ARE ORDERED PAIRS FOR THE RESIDUAL TIME HISTORY	SPEC 308
C		SPEC 309
	$XB(L) = \exp(-DAMP * WD * TT) * (NXP * SWST / WD + NX * CWST)$	SPEC 310
	TB(L)=T	SPEC 311
	XPLT(M)=T	SPEC 312
	YPLT(M)=XB(L)	SPEC 313
	M=M+1	SPEC 314
	L=L+1	SPEC 315
	IF(T.GE.3.*UMAX) GO TO 230	SPEC 316
	T=T+DS	SPEC 317
	GO TO 220	SPEC 318
230	M=M-1	SPEC 319
	IF(IPLT.NE.1) GO TO 240	SPEC 320
	READ(5,1100) TIT4	SPEC 321
C		SPEC 322
C	PLOT TIME HISTORY OF INDIVIDUAL FREQUENCY	SPEC 323
C		SPEC 324
	LST=1	SPEC 325
	LSP=M	SPEC 326
	CALL DATA4(NCURV,XPLT,YPLT,DUM,M,ISC,ITYPE,LST,LSP, * TIT4,ICOLOR)	SPEC 327 SPEC 328
C		SPEC 329
C	THIS SECTION FINDS MAGNITUDE OF PRIMARY TIME HISTORY	SPEC 330
C	(MAXP) AND MAGNITUDE OF RESIDUAL TIME HISTORY (MAXR)	SPEC 331
C		SPEC 332
240	MAXP=XA(1)	SPEC 333
	MAXR=XB(1)	SPEC 334
	DO 250 I=1,L	SPEC 335
	IF(XA(I).LE.MAXP) GO TO 250	SPEC 336
	MAXP=XA(I)	SPEC 337
250	CONTINUE	SPEC 338
	DO 260 I=1,L	SPEC 339
	IF(XB(I).LE.MAXR) GO TO 260	SPEC 340
	MAXR=XB(I)	SPEC 341
260	CONTINUE	SPEC 342
C		SPEC 343
C	THIS SECTION STORES DATA FOR 3-D PLOT	SPEC 344
C		SPEC 345
	MSAVE(NP)=M	SPEC 346
	IF(NP.EQ.1.AND.I3D.EQ.1) WRITE(2)DS	SPEC 347

C	IF (I3D.EQ.1) WRITE(2) M,(XPLT(I),I=1,M),(YPLT(I),I=1,M)	SPEC 348
		SPEC 349
C	IF(IFREQ.EQ.1) F=(F*UMAX)/TCAL	SPEC 350
C		SPEC 351
C	THIS SECTION CONVERTS FREQUENCY TIMES PULSE	SPEC 352
C	DURATION(FT) TO FREQUENCY, IF DESIRED, AND CONVERTS	SPEC 353
C	FT TO LOG10 SCALE, IF DESIRED, AND STORES IT	SPEC 354
C	ALONG WITH MAXR AND XMAX FOR PLOTTING.	SPEC 355
C		SPEC 356
	IF(IFREQ.EQ.1) FT=FT/TCAL	SPEC 357
	IF(ILOG.NE.1) PFT(NP)=FT	SPEC 358
	IF(ILOG.EQ.1) PFT(NP)=ALOG10(FT)	SPEC 359
	RMAX(NP)=MAXR	SPEC 360
	FR(NP)=F	SPEC 361
	FWN(NP)=F0/TCAL	SPEC 362
	PXP(NP)=MAXP	SPEC 363
	PXR(NP)=MAXR	SPEC 364
	NP=NP+1	SPEC 365
C		SPEC 366
C	AFTER THE CODE COMPUTES THE SPECTRUM FOR FMAX, IT	SPEC 367
C	GOES TO THE PLOT SUBROUTINE. OTHERWISE, IT RESETS T,	SPEC 368
C	I, AND S AND RETURNS TO LOCATION 90.	SPEC 369
C		SPEC 370
	IF(F0.GE.FMAX) GO TO 270	SPEC 371
	T=0	SPEC 372
	I=1	SPEC 373
	S=0	SPEC 374
	GO TO 90	SPEC 375
C		SPEC 376
C	NP IS NO. OF FREQUENCIES USED. IT IS RESTRICTED TO	SPEC 377
C	200 DUE TO DIMENSION STATEMENT	SPEC 378
C		SPEC 379
270	NP=NP-1	SPEC 380
C		SPEC 381
C	PLOT PRIMARY AND RESIDUAL SPECTRA	SPEC 382
C		SPEC 383
	IF(ISPEC.NE.1) GO TO 280	SPEC 384
	READ(5,1100) TIT4	SPEC 385
	ITYPE=1	SPEC 386
	LST=1	SPEC 387
	LSP=NP	SPEC 388
	NCURV=2	SPEC 389
	ISC=1	SPEC 390
	IF(ISPEC.EQ.1)CALL DATA4(NCURV,PFT,XPX,PXR,NP,ISC,	SPEC 391
	*ITYPE,LST,LSP,TIT4,ICOLOR)	SPEC 392
	IF(IRES.EQ.1) NCURV=1	SPEC 393
	IF(IRES.EQ.1) CALL DATA4(NCURV,PFT,PXR,DUM,NP,ISC,	SPEC 394
	*ITYPE,LST,LSP,TIT4,ICOLOR)	SPEC 395
	ITYPE=0	SPEC 396
	ISC=0	SPEC 397

C		SPEC 398
C	PRINT HEADINGS AND DATA	SPEC 399
C		SPEC 400
280	WRITE(6,1200) PGTIT	SPEC 401
	WRITE(6,1900)	SPEC 402
	WRITE(6,2000)	SPEC 403
	IF(IFREQ.EQ.1) WRITE(6,2100)	SPEC 404
	IF(IFREQ.NE.1) WRITE(6,2200)	SPEC 405
	WRITE(6,2500) (FR(I),PXP(I),RMAX(I),FWN(I),I=1,NP)	SPEC 406
	WRITE(6,2300) NP	SPEC 407
	REWIND 2	SPEC 408
	DO 290 I=1,1000	SPEC 409
	V(I)=0.0	SPEC 410
	VP(I)=0.	SPEC 411
290	CONTINUE	SPEC 412
	GO TO 10	SPEC 413
300	WRITE(6,2400) T	SPEC 414
	STOP	SPEC 415
1000	FORMAT(2I5,3F10.3,F5.0,5I5,3I2)	SPEC 416
1100	FORMAT(10A8)	SPEC 417
1200	FORMAT(1H1,10A8,/)	SPEC 418
1300	FORMAT(1H0,4(6X,'TIME',7X,'ACCELERATION',1X))	SPEC 419
1400	FORMAT(1H ,4(6X,4HMSEC,11X,3HG'S,6X)/)	SPEC 420
1500	FORMAT(8(1X,F14.5))	SPEC 421
1600	FORMAT(8F10.3)	SPEC 422
1700	FORMAT(1H1,'NORMALIZED INPUT DATA'/)	SPEC 423
1800	FORMAT(2F10.3,I5)	SPEC 424
1900	FORMAT(' PRIMARY AND RESIDUAL SPECTRA OF	SPEC 425
	*ACCELERATION PULSE',/)	SPEC 426
2000	FORMAT(' FREQUENCY',5X,' RELATIVE	SPEC 427
	* ACCELERATION ACTUAL')	SPEC 428
2100	FORMAT(' KHZ',13X,'PRIMARY RESIDUAL	SPEC 429
	*FREQUENCY')	SPEC 430
2200	FORMAT(' X PULSE DURATION',5X,' PRIMARY	SPEC 431
	* RESIDUAL FREQUENCY')	SPEC 432
2300	FORMAT('0NFILES = ',I5)	SPEC 433
2400	FORMAT('0T<0 OR > UMAX+H, T=',F10.3)	SPEC 434
2500	FORMAT(F12.3,5X,3F12.5)	SPEC 435
	END	SPEC 436
C		
C		
C		
	SUBROUTINE DATA4(NCURV,Z1,Z2,Z3,NPLT,ISC,ITYPE,LST,	DATA4 1
	*LSP,TITLE,ICOLOR)	DATA4 2
C		DATA4 3
C	THIS SUBROUTINE SETS UP DATA AND LABELS FOR PLOT	DATA4 4
C		DATA4 5
	DIMENSION Z1(NPLT),Z2(NPLT),X(1000),Y1(1000),DUM(1),	DATA4 6
	*Y2(1000),Z3(NPLT),LXNAME(3),LYNAME(3),TITLE(4)	DATA4 7
	DUM(1)=1.E100	DATA4 8

C		DATA 9
C	STORE DATA TO BE PLOTTED IN APPROPRIATE ARRAYS AND	DATA 10
C	COUNT DATA POINTS	DATA 11
C		DATA 12
	J=0	DATA 13
	DO 100 L=LST,LSP	DATA 14
	J=J+1	DATA 15
	X(J)=Z1(L)	DATA 16
	Y1(J)=Z2(L)	DATA 17
	Y2(J)=Z3(L)	DATA 18
100	CONTINUE	DATA 19
	IF(NCURV.LT.2) Y2(1)=DUM(1)	DATA 20
C		DATA 21
C	PRINT PLOT LIMITS	DATA 22
C		DATA 23
	WRITE(6,2) LST,LSP,X(1),X(J)	DATA 24
C		DATA 25
C	READ AND PRINT PLOT LABELS	DATA 26
C		DATA 27
	READ(5,3) LXNAME,LYNAME	DATA 28
	WRITE(6,3) LXNAME,LYNAME	DATA 29
C		DATA 30
C	CALL PLOT SUBROUTINE	DATA 31
C		DATA 32
	CALL DISS4(X,Y1,Y2,J,TITLE,ISC,ITYPE,LXNAME,LYNAME,	DATA 33
	*ICOLOR)	DATA 34
	RETURN	DATA 35
1	FORMAT(2F10.0)	DATA 36
2	FORMAT(' PLOT LIMITS - ',2I5,2F10.4)	DATA 37
3	FORMAT(10A8)	DATA 38
	END	DATA 39
C		
C		
	SUBROUTINE DISS4(X,Y1,Y2,NPT,TITLE,ISC,ITYPE,LXNAME,	DIS4 1
	*LYNAME,ICOLOR)	DIS4 2
C		DIS4 3
C	THIS SUBROUTINE CREATES A DISSPLA 9 PLOT FILE	DIS4 4
C		DIS4 5
C		DIS4 6
C	ISC=0 SELF-SCALE	DIS4 7
C	=1 READ IN XORIG, XMAX, XSTP, YORIG, YMAX, YSTP	DIS4 8
C		DIS4 9
C	ITYPE=0 NORMAL PLOT	DIS4 10
C	=1 X-LOG AXIS	DIS4 11
C		DIS4 12
C	ICOLOR=0 BLACK/WHITE	DIS4 13
C	=1 COLOR	DIS4 14
C		DIS4 15
	DIMENSION X(NPT),Y1(NPT),Y2(NPT),RAT(10),LXNAME(3),	DIS4 16
	* LYNAME(3),TITLE(4)	DIS4 17

C		DIS4 18
C	DETERMINE PLOT SCALES	DIS4 19
C		DIS4 20
	IF(ISC.NE.0)GO TO 300	DIS4 21
	XORIG=X(1)	DIS4 22
	XSTP='SCALE'	DIS4 23
	XMAX=X(NPT)	DIS4 24
	YORIG=1.E100	DIS4 25
	YSTP='SCALE'	DIS4 26
	YMAX=-1.E100	DIS4 27
	DO 200 I=1,NPT	DIS4 28
	IF(Y1(I).LT.YMAX)GO TO 100	DIS4 29
	YMAX=Y1(I)	DIS4 30
100	IF(Y1(I).GT.YORIG)GO TO 200	DIS4 31
	YORIG=Y1(I)	DIS4 32
200	CONTINUE	DIS4 33
	GO TO 400	DIS4 34
300	READ(5,1)XORIG,XMAX,XSTP,YORIG,YMAX,YSTP	DIS4 35
400	IF(ISC.EQ.1)WRITE(6,2)XORIG,XSTP,XMAX,YORIG,YSTP,YMAX	DIS4 36
	IF(ISC.EQ.0)WRITE(6,2)XORIG,XMAX,YORIG,YMAX	DIS4 37
	JJ=JJ+1	DIS4 38
C		DIS4 39
C	SET UP GRID	DIS4 40
C		DIS4 41
	CALL BASALF('STANDARD')	DIS4 42
	CALL MIXALF('SPECIAL')	DIS4 43
	CALL PHYSOR(1.5,1.)	DIS4 44
	CALL PAGE(11.,8.5)	DIS4 45
	CALL SETCLR('BLACK')	DIS4 46
	XSIZE=8.0	DIS4 47
	YSIZE=6.0	DIS4 48
	CALL AREA2D(XSIZE,YSIZE)	DIS4 49
C		DIS4 50
C	LABEL PLOTS	DIS4 51
C		DIS4 52
	CALL HEIGHT(.25)	DIS4 53
	CALL HEADIN(TITLE,32,1.1,1)	DIS4 54
	CALL XNAME(LXNAME,24)	DIS4 55
	CALL YNAME(LYNAME,24)	DIS4 56
C		DIS4 57
C	SET PLOT SCALES FOR LOG PLOT	DIS4 58
C		DIS4 59
	IF(ITYPE.NE.1) GO TO 500	DIS4 60
	ICY=ALOG10(X(NPT))-ALOG10(X(1))+.5	DIS4 61
	XCY=XSIZE/FLOAT(ICY)	DIS4 62
	IF(ITYPE.EQ.1.AND.ISC.EQ.0)YSTP=(YMAX-YORIG)/YSIZE	DIS4 63
	WRITE(6,3) XCY,YSTP,ICY	DIS4 64
C		DIS4 65
C	DRAW GRID	DIS4 66
C		DIS4 67

500	IF(ITYPE.EQ.0)CALL GRAF(XORIG,XSTP,XMAX,YORIG,	DIS4 68
	*YSTP,YMAX)	DIS4 69
	IF(ITYPE.EQ.1)CALL XLOG(XORIG,XCY,YORIG,YSTP)	DIS4 70
	IMARK=0	DIS4 71
	IF(ICOLOR.EQ.1)CALL SETCLR('BLUE')	DIS4 72
C		DIS4 73
C	PLOT DATA	DIS4 74
C		DIS4 75
	CALL CURVE(X,Y1,NPT,IMARK)	DIS4 76
	IF(ICOLOR.EQ.1)CALL SETCLR('RED')	DIS4 77
	TL=.5	DIS4 78
	NMRK=10	DIS4 79
	RAT(1)=2.	DIS4 80
	RAT(2)=1.	DIS4 81
	IF(ICOLOR.EQ.0)CALL MRSCOD(TL,NMRK,RAT)	DIS4 82
	IF(Y2(1).NE.1.E100.AND.ITYPE.EQ.0)	DIS4 83
	*CALL CURVE(X,Y2,NPT,IMARK)	DIS4 84
	IF(Y2(1).NE.1.E100.AND.ITYPE.EQ.1)	DIS4 85
	*CALL CURVE(X,Y2,NPT,IMARK)	DIS4 86
	CALL RESET('DASH')	DIS4 87
	CALL ENDPL(JJ)	DIS4 88
	RETURN	DIS4 89
1	FORMAT(6E10.3)	DIS4 90
2	FORMAT(' PLOT SCALES - ',6E13.5)	DIS4 91
3	FORMAT(' XCYCLE, YSTP, ICY =',2E13.5,I10)	DIS4 92
	END	DIS4 93

APPENDIX B

LISTING OF FORTRAN PROGRAM TO CREATE 3-D SHOCK RESPONSE PLOT
ALONG WITH ASSOCIATED JOB CONTROL LANGUAGE FOR CRAY XMP/48

APPENDIX B

LISTING OF FORTRAN PROGRAM TO CREATE 3-D SHOCK RESPONSE PLOT ALONG WITH ASSOCIATED JOB CONTROL LANGUAGE FOR CRAY XMP/48

I. Job Control Language for CRAY XMP/48

```
JOB,JN=jobname,T=150,MFL=350000.  
ACCOUNT,AC=accountnumber,US=username,UPW=userpassword.  
ACCESS,DN=DISLIB,PDN=DISLIB,ID=DISSPLA,OWN=SYSTEM.  
ACCESS,DN=DVSD,PDN=DVSD,ID=DISSPLA,OWN=SYSTEM.  
ACCESS,DN=INTLIB,PDN=INTLIB,ID=DISSPLA,OWN=SYSTEM.  
FETCH,DN=3dfile,TEXT='CHARGE,acctno,pn.GET,3dfile=3dfile.CTASK.',DF=BB.
```

where *3dfile* = name of input file which contains data for
calculations for 3-D plot

pn = first two letters of account number

```
ASSIGN,DN=3dfile,A=FT01.  
FETCH,DN=infile,TEXT='CHARGE,acctno,pn.GET,infile=infile.CTASK.'
```

where *infile* = name of input file which contains program options
and plot titles

pn = first two letters of the account number

```
ASSIGN,DN=infile,A=FT05.  
CFT.  
SEGLDR,CMD='LIB=DISLIB,INTLIB',GO.  
DISPOSE,DN=META,DC=ST,DF=BB,^  
TEXT='CHARGE=acctno,pn.CTASK.REPLACE,META=pl3file.'
```

where *pl3file* = name of output file in which the DISSPLA plot file
for 3-D plot is stored on the front end.

II. Listing of FORTRAN File

	PROGRAM DUHM3D(INPUT,OUTPUT,TAPE1,TAPE5,	DU3D	1
	* TAPE6=OUTPUT,META,TAPE10=OUTPUT,TAPE2)	DU3D	2
C		DU3D	3
C	THIS PROGRAM READS FREQUENCY RESPONSE DATA AND	DU3D	4
C	CREATES A 3-D SURFACE PLOT	DU3D	5
C		DU3D	6
C	THIS PROGRAM USES A DATA FILE CREATED BY A	DU3D	7
C	DUHAMEL INTEGRAL PROGRAM AS INPUT	DU3D	8

C		DU3D 9
	DIMENSION TX(65),TY(65),TX1(65),TY1(65)	DU3D 10
	DIMENSION TX2(65),TY2(65),TX3(65),TY3(65),TX4(65),TY4(65)	DU3D 11
	DIMENSION OFF(50),OFFX(50),PARRAY(1500,4),RES(1500,4),	DU3D 12
	* T1(4,4),XPT(1500),YPT(1500),TIT4(4),XPLT(1500),YPLT(1500),	DU3D 13
	* T2(4,4)	DU3D 14
C		DU3D 15
	DATA OFF/1.,1.33,1.67,2.,2.5,3.,3.5,4.,5.,6.,7.,8.,9.,10.,13.3,	DU3D 16
	*16.7,20.,25.,30.,35.,40.,50.,60.,70.,80.,90.,100.,133.33,166.67,	DU3D 17
	*200.,250.,300.,350.,400.,500.,600.,700.,800.,900.,1000.,1333.3,	DU3D 18
	*1666.67,2000.,2500.,3000.,4000.,5000.,6000.,7000.,8000./	DU3D 19
C		DU3D 20
C	INITIALIZE DISSPLA	DU3D 21
C		DU3D 22
	CALL COMPRS	DU3D 23
	CALL SETDEV(10,6)	DU3D 24
C		DU3D 25
	ISC=1.	DU3D 26
	ICOLOR=1	DU3D 27
	IEP=1	DU3D 28
C		DU3D 29
C	NFILES(15) = NUMBER OF FREQUENCY RESPONSE CURVES	DU3D 30
C	MAXT (15) = MAXIMUM TIME OF RESPONSE PLOT	DU3D 31
C	MAXT = 1, PRIMARY RESPONSE CURVE	DU3D 32
C	MAXT = 2, PRIMARY RESPONSE PLUS PARTIAL RESIDUAL	DU3D 33
C	MAXT = 3, PRIMARY RESPONSE PLUS FULL RESIDUAL	DU3D 34
C		DU3D 35
	READ(5,1000) NFILES,MAXT	DU3D 36
	NF=NFILES	DU3D 37
C		DU3D 38
C	DS = TIME STEP READ FROM DATA FILE	DU3D 39
C		DU3D 40
	READ(1) DS	DU3D 41
	WRITE(6,5000) DS	DU3D 42
C		DU3D 43
C	CALCULATE NUMBER AND INTERVAL OF TIME CURVES	DU3D 44
C	TO BE PLOTTED	DU3D 45
C		DU3D 46
	K=(MAXT/DS)+1	DU3D 47
	A=MAXT	DU3D 48
	B=AMOD(A,DS)	DU3D 49
	IF(B.GE..0)K=K+1	DU3D 50
	KD=K/4	DU3D 51
	J1=4	DU3D 52
	J=MOD(K,J1)	DU3D 53
	IF(J.GT.0)KD=KD+1	DU3D 54
	KS=K/100	DU3D 55
	J1=100	DU3D 56
	J=MOD(K,J1)	DU3D 57
	IF(J.GT.0)KS=KS+1	DU3D 58

	KD2=2*KD	DU3D 59
	KD3=3*KD	DU3D 60
	KP=0	DU3D 61
	WRITE(6,6000) KD,KS,K	DU3D 62
	IPSAVE=10000	DU3D 63
C		DU3D 64
C	READ DATA AND STORE IN SEPARATE ARRAYS TO CREATE	DU3D 65
C	DATA CURVES AT SPECIFIC TIME INTERVALS	DU3D 66
C		DU3D 67
	DO 80 J=1,KD,KS	DU3D 68
	IS=0	DU3D 69
	DO 60 I=1,NF	DU3D 70
	IS=IS+1	DU3D 71
	IF(J.GT.1.AND.I.EQ.1) READ(1) DS	DU3D 72
	READ(1) M,(XPLT(N),N=1,M),(YPLT(N),N=1,M)	DU3D 73
	IF(I.EQ.1.AND.J.EQ.1)WRITE(6,4000) (XPLT(N),N=1,M),(YPLT(N),N=1,M)	DU3D 74
	IF(J.EQ.1.AND.I.EQ.1) GO TO 30	DU3D 75
10	IF((J+KD2).GT.IPSAVE) KP=1	DU3D 76
	TX(I)=XPLT(J)	DU3D 77
	TY(I)=YPLT(J)	DU3D 78
	TX1(I)=XPLT(J+KD)	DU3D 79
	TY1(I)=YPLT(J+KD)	DU3D 80
	TX2(I)=XPLT(J+KD2+KP)	DU3D 81
	TY2(I)=YPLT(J+KD2+KP)	DU3D 82
	TX3(I)=XPLT(J+KD3+KP)	DU3D 83
	TY3(I)=YPLT(J+KD3+KP)	DU3D 84
	IF((J+KS).GT.KD.AND.J.NE.KD) GO TO 20	DU3D 85
	GO TO 60	DU3D 86
20	IF(I.EQ.1) IEND=1	DU3D 87
	TX4(I)=XPLT(K)	DU3D 88
	TY4(I)=YPLT(K)	DU3D 89
	GO TO 60	DU3D 90
30	K1=1	DU3D 91
	DO 40 IP=1,M	DU3D 92
	IF((XPLT(IP+1)-XPLT(IP)).LT..001) IPSAVE=IP	DU3D 93
	IF(ABS(MAXT-XPLT(IP)).LT..0001) GO TO 50	DU3D 94
	K1=K1+1	DU3D 95
40	CONTINUE	DU3D 96
50	K=K1	DU3D 97
	GO TO 10	DU3D 98
60	CONTINUE	DU3D 99
	REWIND 1	DU3D 100
C		DU3D 101
C	STORE NEWLY CREATED DATA CURVES	DU3D 102
C		DU3D 103
	WRITE(2) IS,(TX(N),N=1,IS),(TY(N),N=1,IS)	DU3D 104
	NFILES=NFILES+1	DU3D 105
	WRITE(2) (TX1(N),N=1,IS),(TY1(N),N=1,IS)	DU3D 106
	NFILES=NFILES+1	DU3D 107
	WRITE(2) (TX2(N),N=1,IS),(TY2(N),N=1,IS)	DU3D 108

	NFILES = NFILES + 1	DU3D 109
	WRITE(2) (TX3(N),N=1,IS),(TY3(N),N=1,IS)	DU3D 110
	NFILES = NFILES + 1	DU3D 111
	WRITE(6,4000) (TX(N),N=1,8),(TY(N),N=1,8)	DU3D 112
	IF (IEND.NE.1) GO TO 70	DU3D 113
	WRITE(2) (TX4(N),N=1,IS),(TY4(N),N=1,IS)	DU3D 114
	NFILES = NFILES + 1	DU3D 115
70	WRITE(6,2000) J	DU3D 116
	IF (IEND.EQ.1) WRITE(6,3000)	DU3D 117
80	CONTINUE	DU3D 118
	REWIND 2	DU3D 119
C		DU3D 120
C	GENERATE OFFSET FACTORS FOR PLOTTING	DU3D 121
C		DU3D 122
	RMS = (ALOG10(OFF(NF)) - ALOG10(OFF(1))) / (NF * .01)	DU3D 123
	DO 90 I = 1, NF	DU3D 124
	OFFX(I) = (ALOG10(OFF(NF)) - ALOG10(OFF(I)) - NF * .01 * RMS) / (-RMS)	DU3D 125
90	CONTINUE	DU3D 126
C		DU3D 127
C	SET UP ARRAYS FOR CURVE ROTATION	DU3D 128
C		DU3D 129
	AX = 1HY	DU3D 130
	ANG = 53	DU3D 131
	CALL ROT1 (ANG,AX,T1)	DU3D 132
	AX = 1HX	DU3D 133
	ANG = 67	DU3D 134
	CALL ROT1 (ANG,AX,T2)	DU3D 135
C		DU3D 136
C	READ DATA FROM FILES	DU3D 137
C		DU3D 138
	IMAXC = NFILES	DU3D 139
	DO 180 II = 1, NFILES	DU3D 140
	J1 = 4	DU3D 141
	J = MOD((II - NF), J1)	DU3D 142
	MM = 1	DU3D 143
	IF (II.GT.NF) GO TO 100	DU3D 144
	IF (II.EQ.1) READ(1) DS	DU3D 145
	READ(1) M, (XPLT(I), I = 1, M), (YPLT(I), I = 1, M)	DU3D 146
	GO TO 120	DU3D 147
100	IF (J.EQ.1.AND.II.NE.NFILES) GO TO 110	DU3D 148
	READ(2) (XPLT(I), I = 1, M), (YPLT(I), I = 1, M)	DU3D 149
	GO TO 120	DU3D 150
110	READ(2) M, (XPLT(I), I = 1, M), (YPLT(I), I = 1, M)	DU3D 151
C		DU3D 152
C	ROTATE DATA	DU3D 153
C		DU3D 154
120	DO 130 JJ = 1, M	DU3D 155
	PARRAY(MM, 2) = YPLT(JJ)	DU3D 156
	PARRAY(MM, 1) = XPLT(JJ)	DU3D 157
	PARRAY(MM, 3) = 0.	DU3D 158

	PARRAY(MM,4)=1.	DU3D 159
	MM=MM+1	DU3D 160
	IF(II.GT.NF) GO TO 130	DU3D 161
	IF(XPLT(JJ).GE.MAXT) GO TO 140	DU3D 162
130	CONTINUE	DU3D 163
140	MM=MM-1	DU3D 164
	IA=MM	DU3D 165
	IM=1500	DU3D 166
	JM=4	DU3D 167
	KM=4	DU3D 168
	NM=1500	DU3D 169
	CALL MATMPY(PARRAY,T1,RES,IA,JM,KM,IM,JM,NM)	DU3D 170
	CALL MATMPY(RES,T2,PARRAY,IA,JM,KM,IM,JM,NM)	DU3D 171
C		DU3D 172
C	OFFSET DATA FOR PLOTTING	DU3D 173
C		DU3D 174
	DO 170 JJ=1,MM	DU3D 175
	IF(II.LE.NF) GO TO 150	DU3D 176
	OFFSETX=OFFX(JJ)	DU3D 177
	OFFSET=OFF(JJ)	DU3D 178
	IF(IEND.EQ.1.AND.II.EQ.NFILES.AND.JJ.EQ.MM)OFFSET=OFF(50)	DU3D 179
	GO TO 160	DU3D 180
150	OFFSETX=OFFX(II)	DU3D 181
	OFFSET=OFF(II)	DU3D 182
160	XPT(JJ)=PARRAY(JJ,1)+OFFSETX	DU3D 183
	YPT(JJ)=PARRAY(JJ,2)-ALOG10(OFFSET)	DU3D 184
170	CONTINUE	DU3D 185
C		DU3D 186
C	READ PLOT TITLE AND CALL PLOT ROUTINE	DU3D 187
C		DU3D 188
	IF(IEP.EQ.1) READ(5,7000) TIT4	DU3D 189
	LST=1	DU3D 190
	LSP=MM	DU3D 191
	NPLT=1500	DU3D 192
	CALL DATA4(XPT,YPT,NPLT,ISC,LST,LSP,TIT4,ICOLOR,IEP,IMAXC)	DU3D 193
	IEP=IEP+1	DU3D 194
180	CONTINUE	DU3D 195
	CALL DONEPL	DU3D 196
1000	FORMAT(2I5)	DU3D 197
2000	FORMAT(' CYCLE NO. ',I5,' HAS BEEN STORED')	DU3D 198
3000	FORMAT(' FINAL FILE HAS BEEN STORED')	DU3D 199
4000	FORMAT(8F12.5)	DU3D 200
5000	FORMAT('0DS= ',F30.20)	DU3D 201
6000	FORMAT(' KD KS K ',3I10)	DU3D 202
7000	FORMAT(10A8)	DU3D 203
	STOP	DU3D 204
	END	DU3D 205
C		
	SUBROUTINE ROT1(ANG,AX,T)	ROT1 1

C		ROT1 2
C	THIS SUBROUTINE CREATES A MATRIX FOR ROTATION OF DATA	ROT1 3
C		ROT1 4
C		ROT1 5
	DIMENSION T(4,4)	ROT1 6
C		ROT1 7
C	CONVERT DEGREES TO RADIANS	ROT1 8
C		ROT1 9
	ANG=ANG*.01745329	ROT1 10
C		ROT1 11
C	ZEROING OUT THE T ARRAY	ROT1 12
C		ROT1 13
	DO 100 I=1,4	ROT1 14
	DO 100 J=1,4	ROT1 15
	T(I,J)=0.0	ROT1 16
100	CONTINUE	ROT1 17
	IF(AX.EQ.1HY) GO TO 200	ROT1 18
	IF(AX.EQ.1HZ) GO TO 300	ROT1 19
C		ROT1 20
C	X-AXIS ARRAY	ROT1 21
C		ROT1 22
	T(2,3)=SIN(ANG)	ROT1 23
	T(2,2)=COS(ANG)	ROT1 24
	T(3,2)=-T(2,3)	ROT1 25
	T(3,3)=T(2,2)	ROT1 26
	T(1,1)=1.	ROT1 27
	GO TO 400	ROT1 28
C		ROT1 29
C	Y-AXIS ARRAY	ROT1 30
C		ROT1 31
200	T(3,1)=SIN(ANG)	ROT1 32
	T(1,1)=COS(ANG)	ROT1 33
	T(1,3)=-T(3,1)	ROT1 34
	T(3,3)=T(1,1)	ROT1 35
	T(2,2)=1.	ROT1 36
	GO TO 400	ROT1 37
C		ROT1 38
C	Z-AXIS ARRAY	ROT1 39
C		ROT1 40
300	T(1,3)=SIN(ANG)	ROT1 41
	T(1,1)=COS(ANG)	ROT1 42
	T(2,1)=-T(1,3)	ROT1 43
	T(2,2)=T(1,1)	ROT1 44
	T(3,3)=1.	ROT1 45
400	RETURN	ROT1 46
	END	ROT1 47
C		
	SUBROUTINE DATA4(Z1,Z2,NPLT,ISC,LST,LSP,TITLE,ICOLOR,	DATA4 1
	*IEP,IMAXC)	DATA4 2

C		DATA4 3
C	THIS SUBROUTINE SETS UP DATA FOR PLOTTING	DATA4 4
C	AND CREATES A 3-D DISSPLA 9 PLOT FILE	DATA4 5
C		DATA4 6
	DIMENSION Z1(NPLT),Z2(NPLT),X(1000),Y1(1000),TITLE(4)	DATA4 7
C		DATA4 8
C	ISC=0 SELF-SCALE	DATA4 9
C	=1 READ IN XORIG, XMAX, XSTP, YORIG, YMAX, YSTP	DATA4 10
C		DATA4 11
C	ICOLOR=0 BLACK/WHITE	DATA4 12
C	=1 COLOR	DATA4 13
C		DATA4 14
C		DATA4 15
C	STORE DATA TO BE PLOTTED IN APPROPRIATE ARRAYS AND	DATA4 16
C	COUNT DATA POINTS	DATA4 17
C		DATA4 18
	J=0	DATA4 19
	DO 10 L=LST,LSP	DATA4 20
	J=J+1	DATA4 21
	X(J)=Z1(L)	DATA4 22
	Y1(J)=Z2(L)	DATA4 23
10	CONTINUE	DATA4 24
C		DATA4 25
C	PRINT PLOT LIMITS	DATA4 26
C		DATA4 27
	WRITE(6,3000)LST,LSP,X(1),X(J)	DATA4 28
	NPT=J	DATA4 29
	IF(IEP.GT.1) GO TO 60	DATA4 30
C		DATA4 31
C	DETERMINE PLOT SCALES	DATA4 32
C		DATA4 33
	IF(ISC.NE.0)GO TO 40	DATA4 34
	XORIG=X(1)	DATA4 35
	XSTP='SCALE'	DATA4 36
	XMAX=X(NPT)	DATA4 37
	YORIG=1.E100	DATA4 38
	YSTP='SCALE'	DATA4 39
	YMAX=-1.E100	DATA4 40
	DO 30 I=1,NPT	DATA4 41
	IF(Y1(I).LT.YMAX)GO TO 20	DATA4 42
	YMAX=Y1(I)	DATA4 43
20	IF(Y1(I).GT.YORIG)GO TO 30	DATA4 44
	YORIG=Y1(I)	DATA4 45
30	CONTINUE	DATA4 46
	GO TO 50	DATA4 47
40	READ(5,1000)XORIG,XMAX,XSTP,YORIG,YMAX,YSTP	DATA4 48
50	IF(ISC.EQ.1)WRITE(6,2000)XORIG,XSTP,XMAX,YORIG,YSTP,YMAX	DATA4 49
	IF(ISC.EQ.0)WRITE(6,2000)XORIG,XMAX,YORIG,YMAX	DATA4 50
	JJ=JJ+1	DATA4 51
C		DATA4 52

C	SET UP PLOTTING AREA	DAT4 53
C		DAT4 54
	CALL PHYSOR(1.5,1.)	DAT4 55
	CALL NOBRDR	DAT4 56
	CALL PAGE(11.,8.5)	DAT4 57
	CALL SETCLR('BLACK')	DAT4 58
	XSIZE=9.0	DAT4 59
	YSIZE=6.0	DAT4 60
	CALL AREA2D(XSIZE,YSIZE)	DAT4 61
C		DAT4 62
C	PLOT TITLE	DAT4 63
C		DAT4 64
	CALL HEIGHT(.25)	DAT4 65
	CALL HEADIN(TITLE,32,1.1,1)	DAT4 66
	CALL GRAF(XORIG,XSTP,XMAX,YORIG,YSTP,YMAX)	DAT4 67
	IMARK=0	DAT4 68
	IF(ICOLOR.EQ.1)CALL SETCLR('BLUE')	DAT4 69
C		DAT4 70
C	PLOT DATA	DAT4 71
C		DAT4 72
60	CALL CURVE(X,Y1,NPT,IMARK)	DAT4 73
	IF(IMAXC.EQ.IEP) CALL ENDPL(JJ)	DAT4 74
	RETURN	DAT4 75
1000	FORMAT(6E10.3)	DAT4 76
2000	FORMAT(' PLOT SCALES - ',6E13.5)	DAT4 77
3000	FORMAT(' PLOT LIMITS - ',2I5,2F10.4)	DAT4 78
	END	DAT4 79
C		
	SUBROUTINE MATMPY (A,B,C,I,J,K,L,M,N)	MATMPY 1
C		MATMPY 2
C	A(I,J) B(J,K) ARE ACTUAL DIMENSIONS WITHIN	MATMPY 3
C	MAX DIMENSIONS OF A(L,) B(M,) C(N,)	MATMPY 4
C	REST OF RESULT C IS NOT SET TO ZERO	MATMPY 5
C		MATMPY 6
	DIMENSION A(L,J),B(M,K),C(N,K)	MATMPY 7
	DO 2 I2=1,K	MATMPY 8
	DO 2 I1=1,I	MATMPY 9
	C(I1,I2)=0.	MATMPY 10
	DO 2 I3=1,J	MATMPY 11
2	C(I1,I2)=C(I1,I2)+A(I1,I3)*B(I3,I2)	MATMPY 12
	RETURN	MATMPY 13
	END	MATMPY 14

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